

VARIABLE VOLUME SYSTEMS

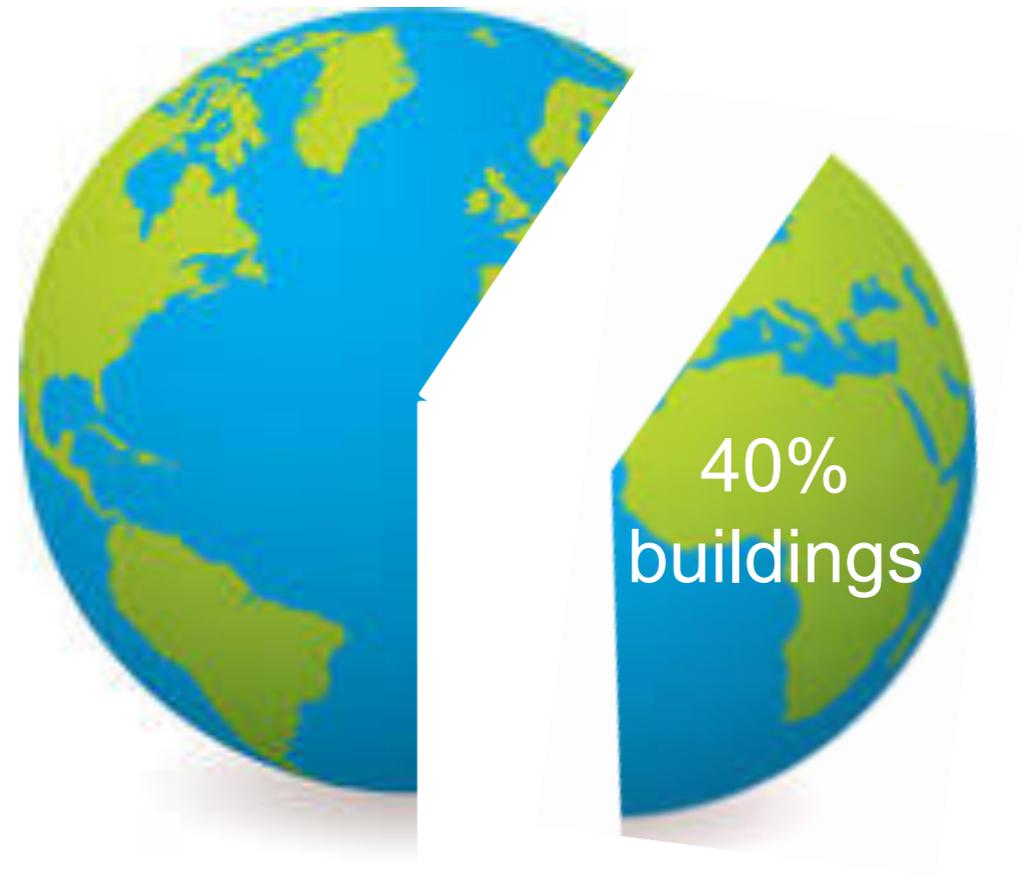
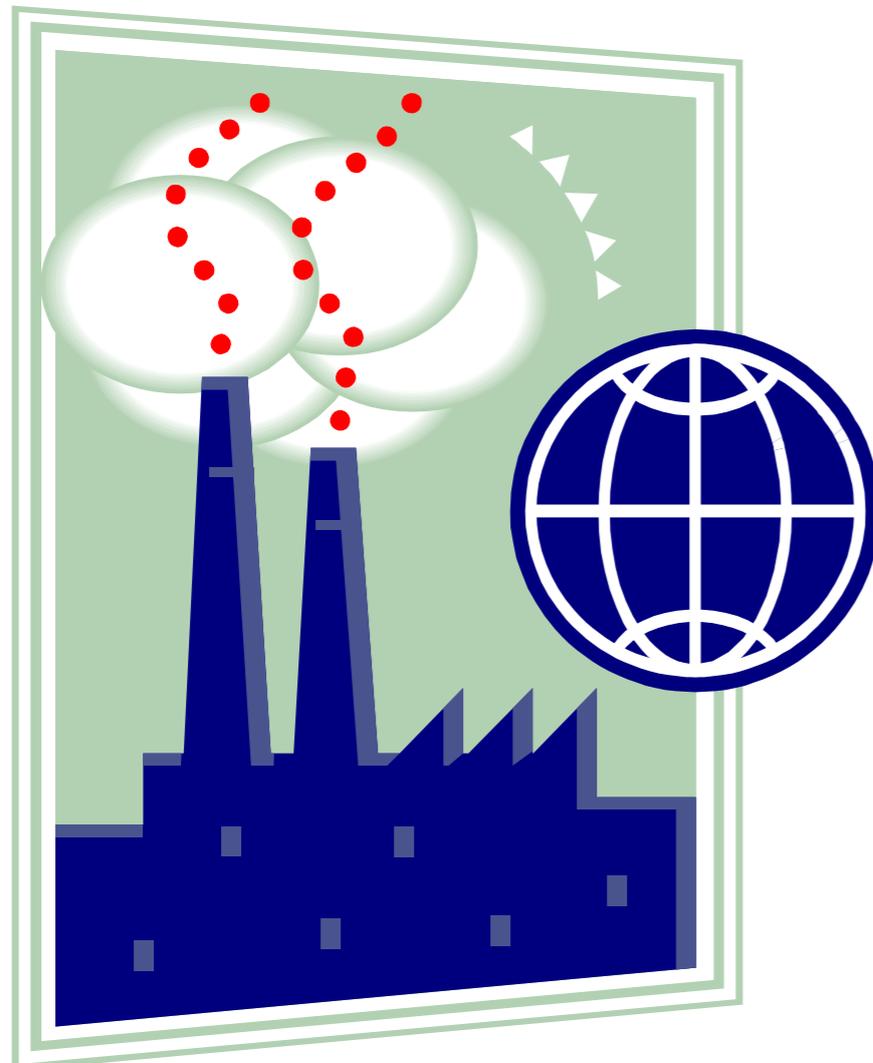


The Bigger Energy Issue

- Environment
- Climate change
- CO₂ emissions
- Who is the biggest culprit?
 - Cars?
 - Planes?
 - No, actually, it's buildings



World Energy Consumption

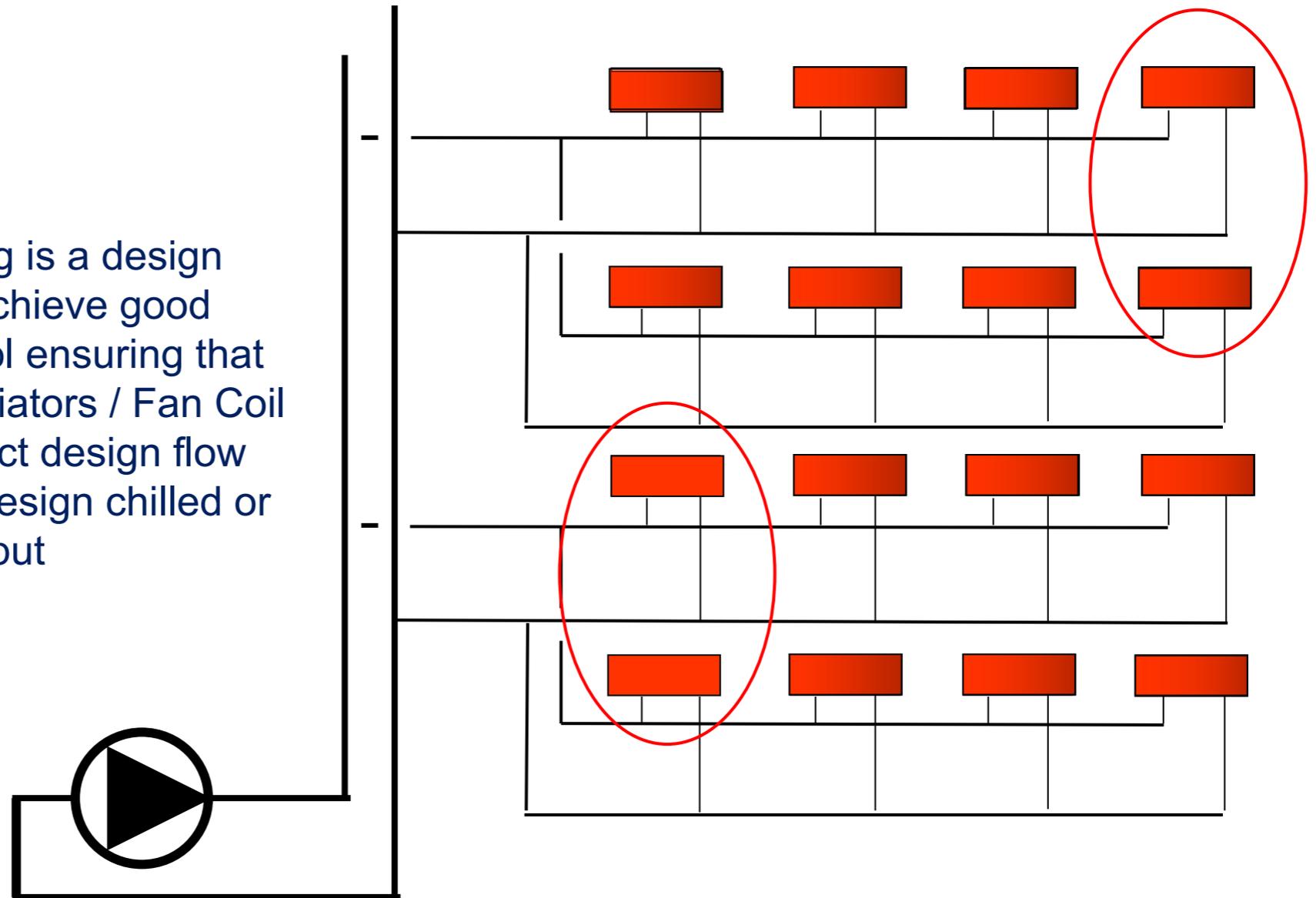


40% of world energy consumption goes into buildings

Alleviating the Energy issue: Dynamic Balancing

Dynamic Balancing is a design methodology to achieve good environmental control ensuring that all terminal units (Radiators / Fan Coil Units etc.) get correct design flow rates and therefore design chilled or heat output

unbalanced
balanced



Why do we need Dynamic Balancing?

Move from Constant Volume to Variable Volume systems

- driven by Government legislation
- energy conservation
- subsequent CO₂ emissions

The move from constant to variable flow design enables pump energy savings

Why do we need Dynamic Balancing – constant volume

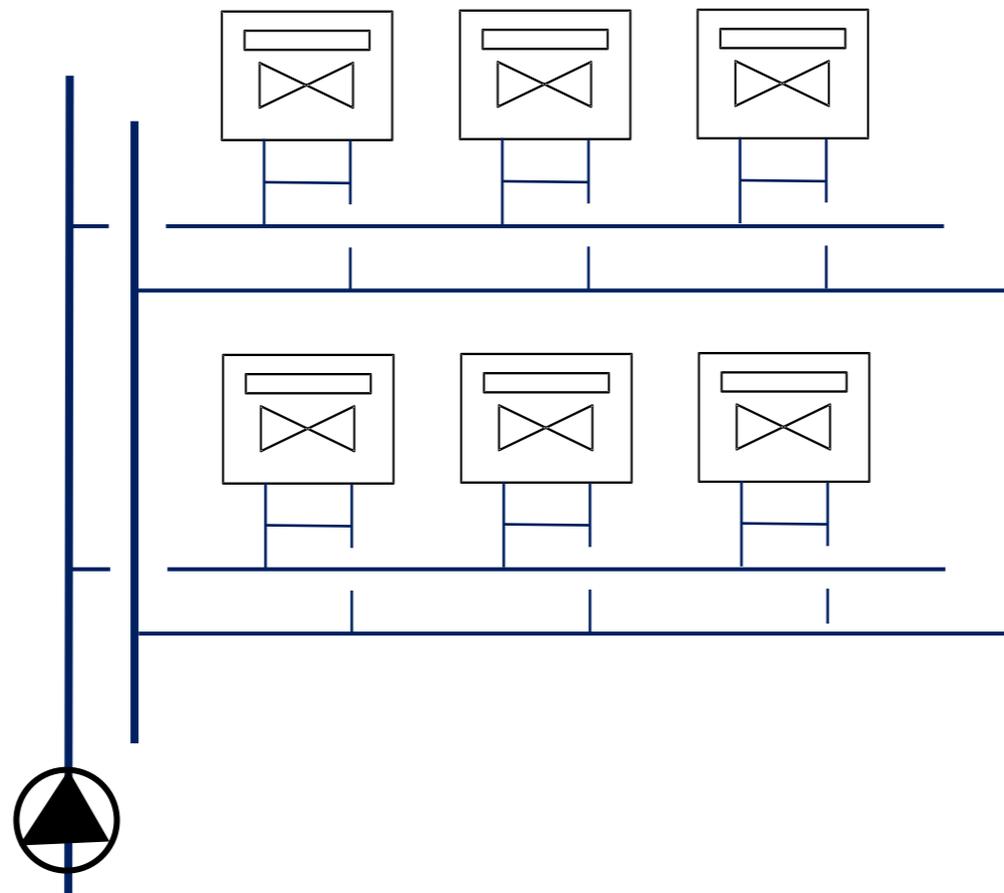
inherently very *stable*

constant pressure drops in distribution pipework

constant pressure drops in circuits at part load

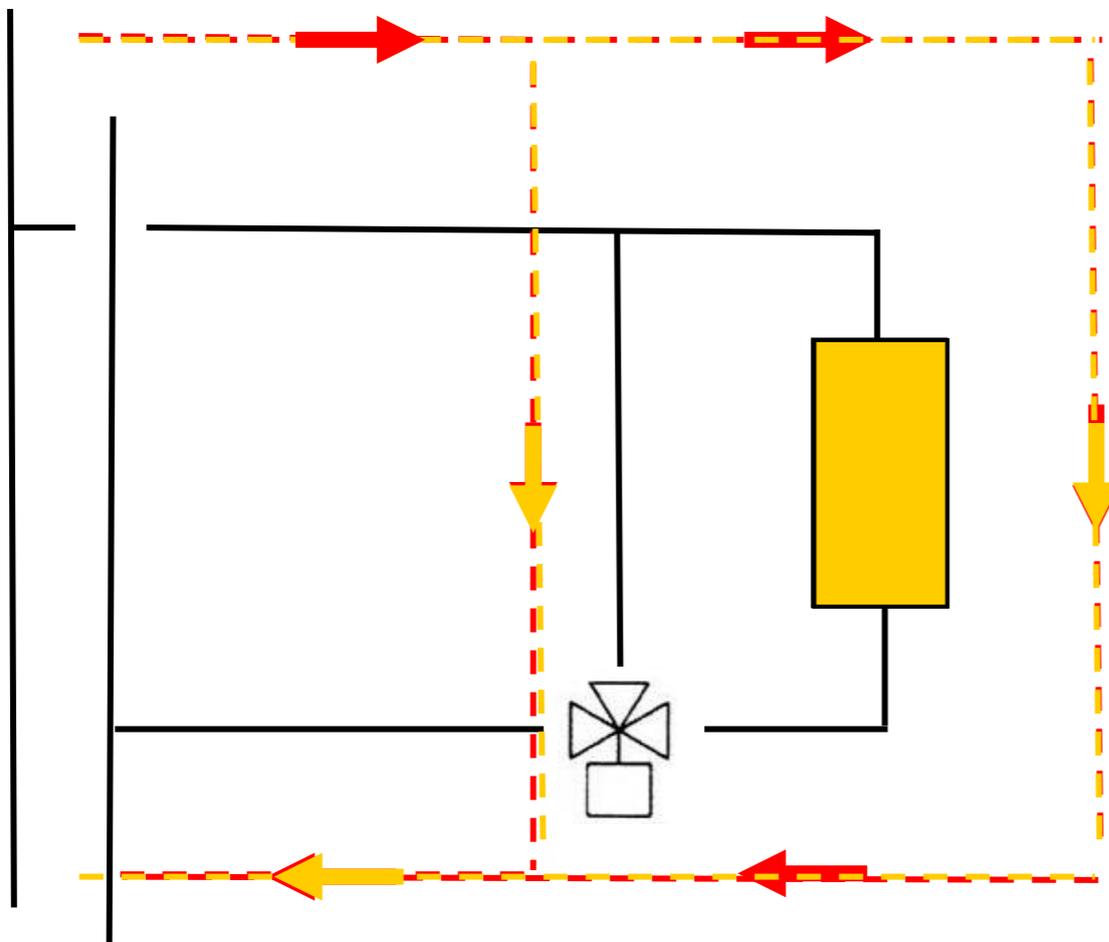
constant pump head

constant control valve authority



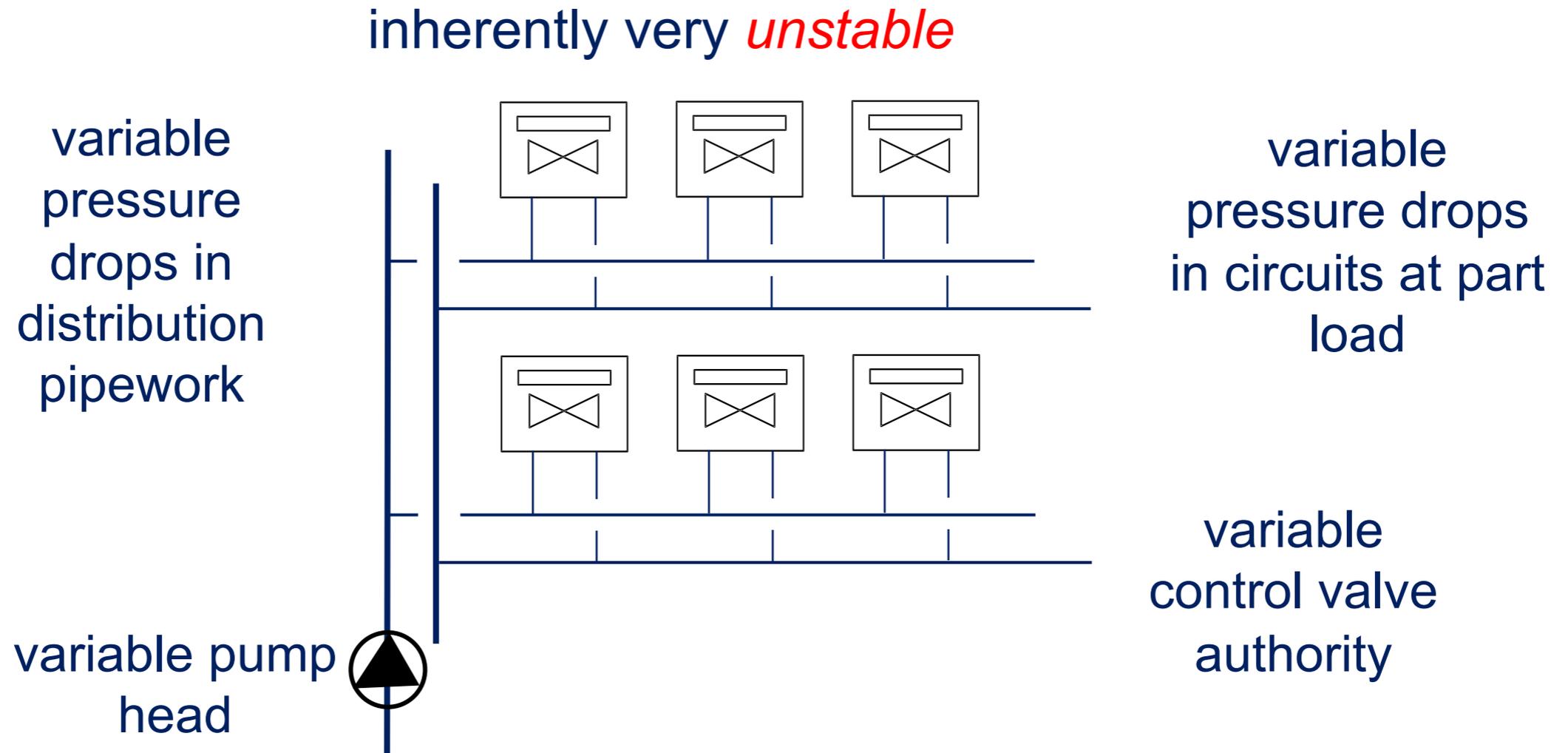
Control valves easy to size with constant authority

Why do we need Dynamic Balancing – constant volume



- constant amount of water pumped around a system controlled by 3 or 4 port control valves and would be
- through terminal
 - split between terminal and by-pass
 - diverted back if not required

Why do we need Dynamic Balancing – variable volume

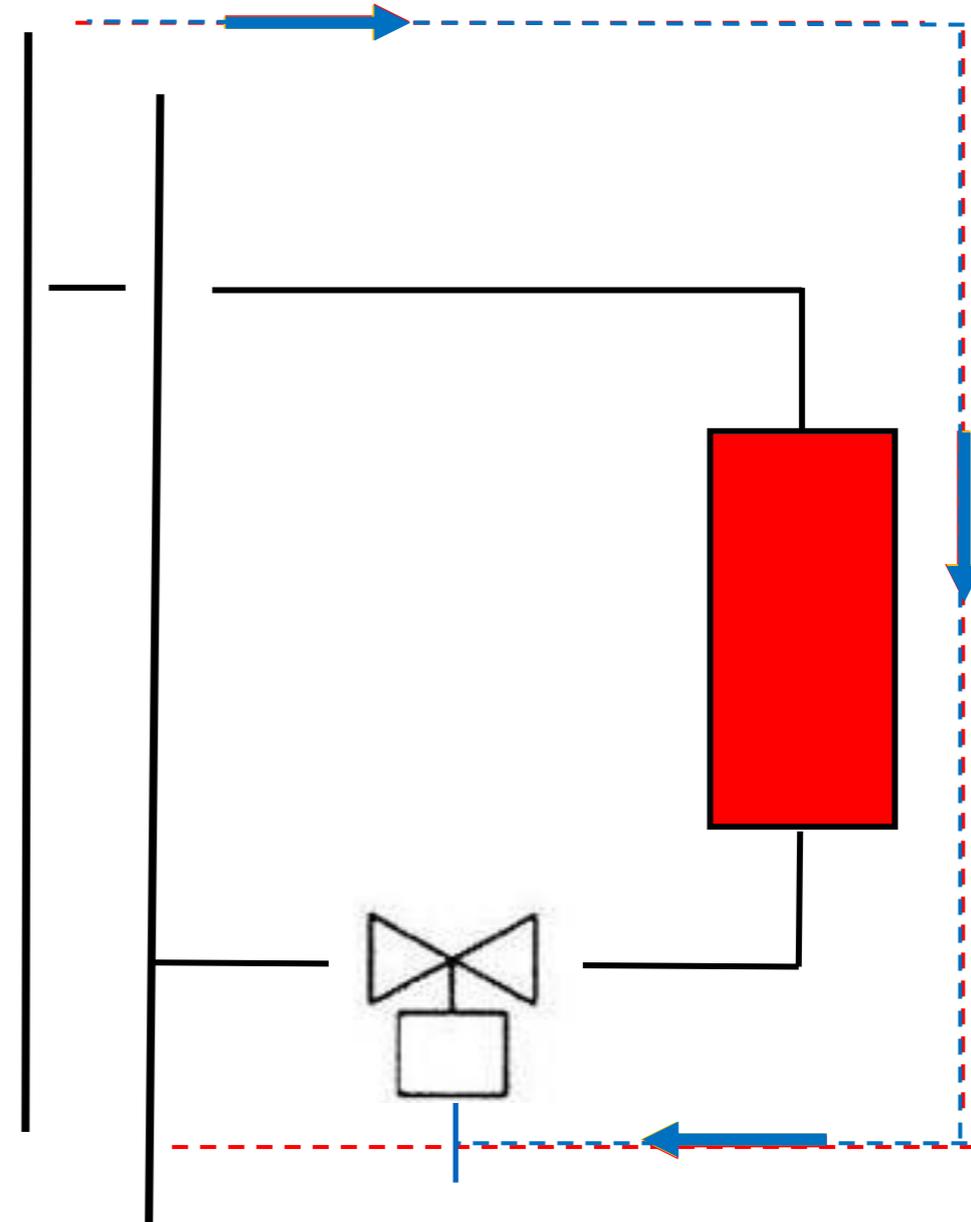


Control valves difficult to size with variable authority

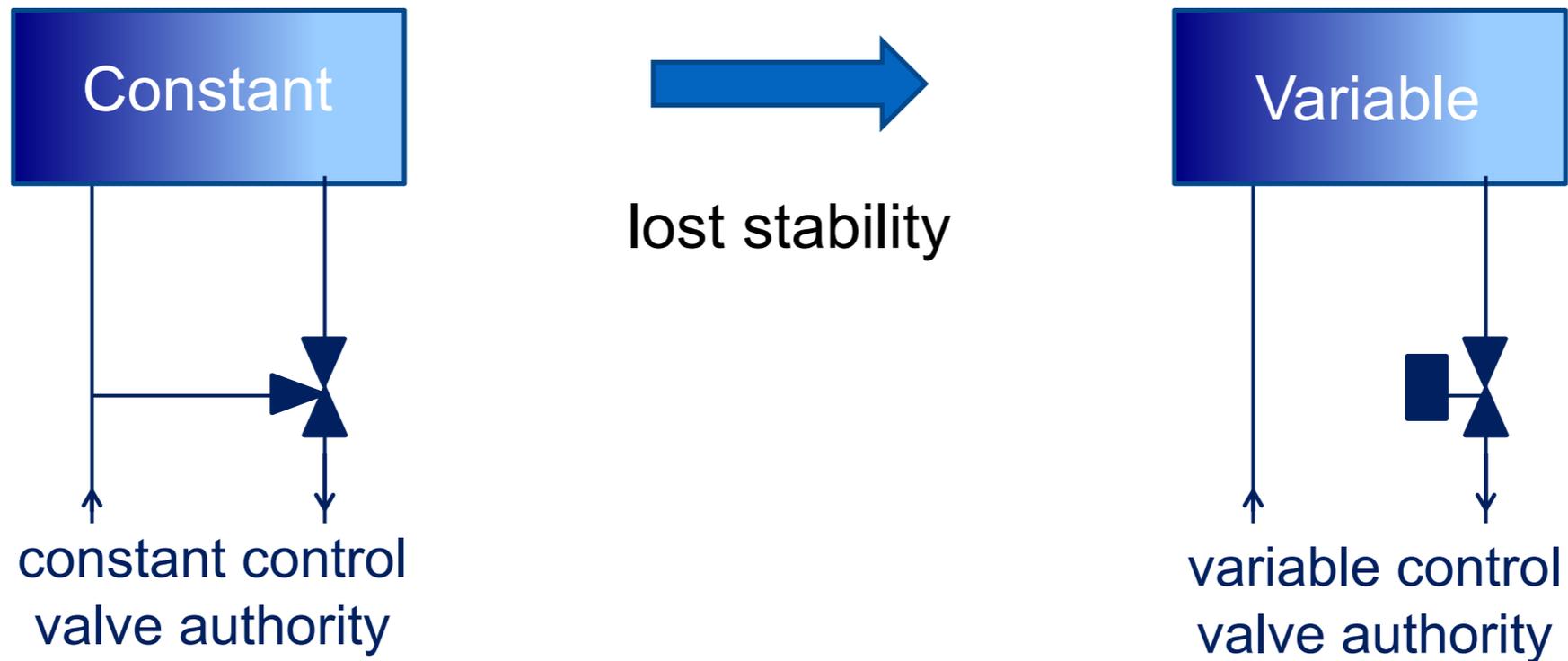
Why do we need Dynamic Balancing – variable volume

Variable amount of water pumped around a system now controlled by 2 port control valves

open
Modulating between open and closed
closed



Why do we need Dynamic Balancing Valves

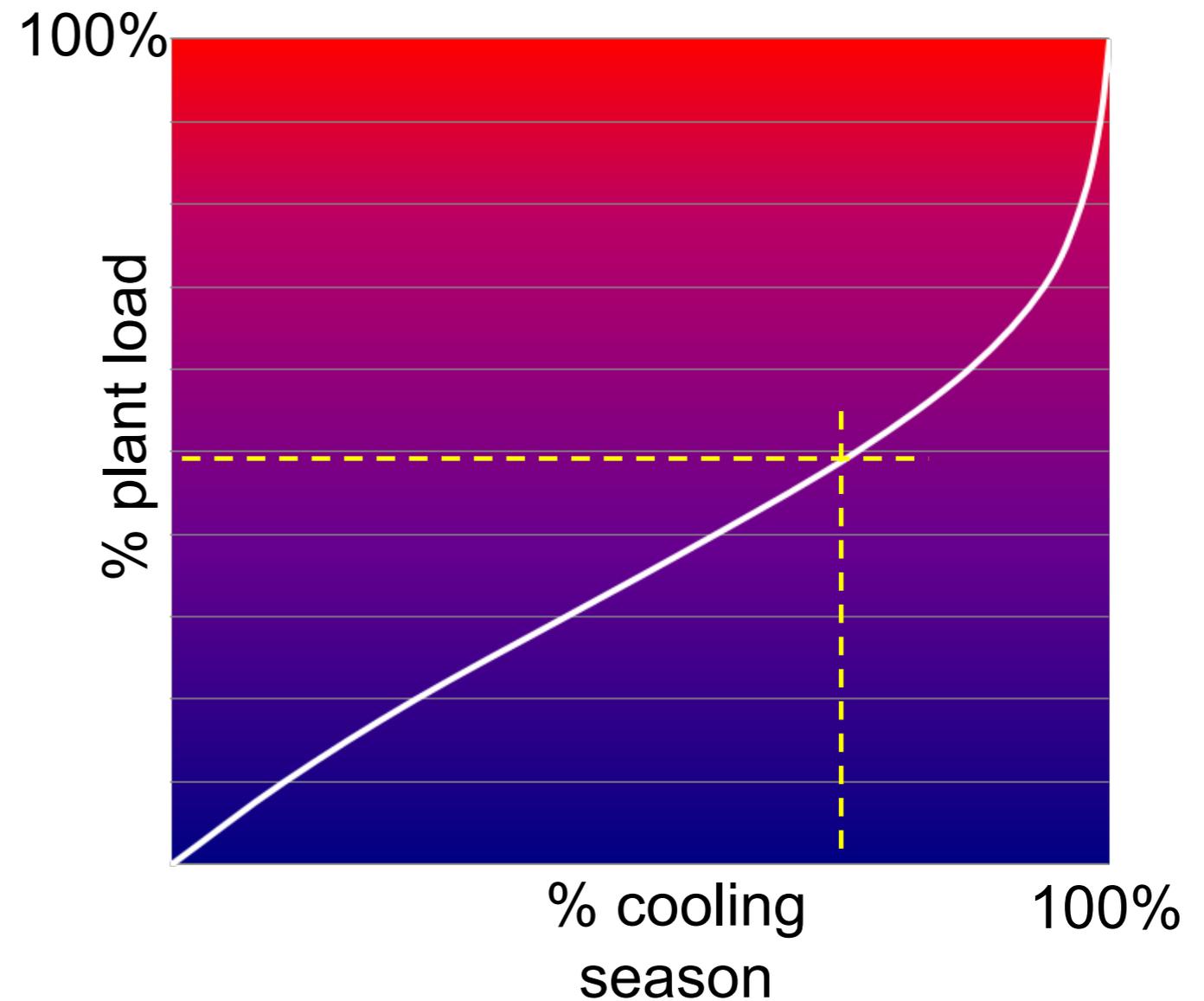


***DPCV installed to protect 2 port control valve authority
or
PICVs installed to replace commissioning / control valves***

Why do we need Variable Volume Systems

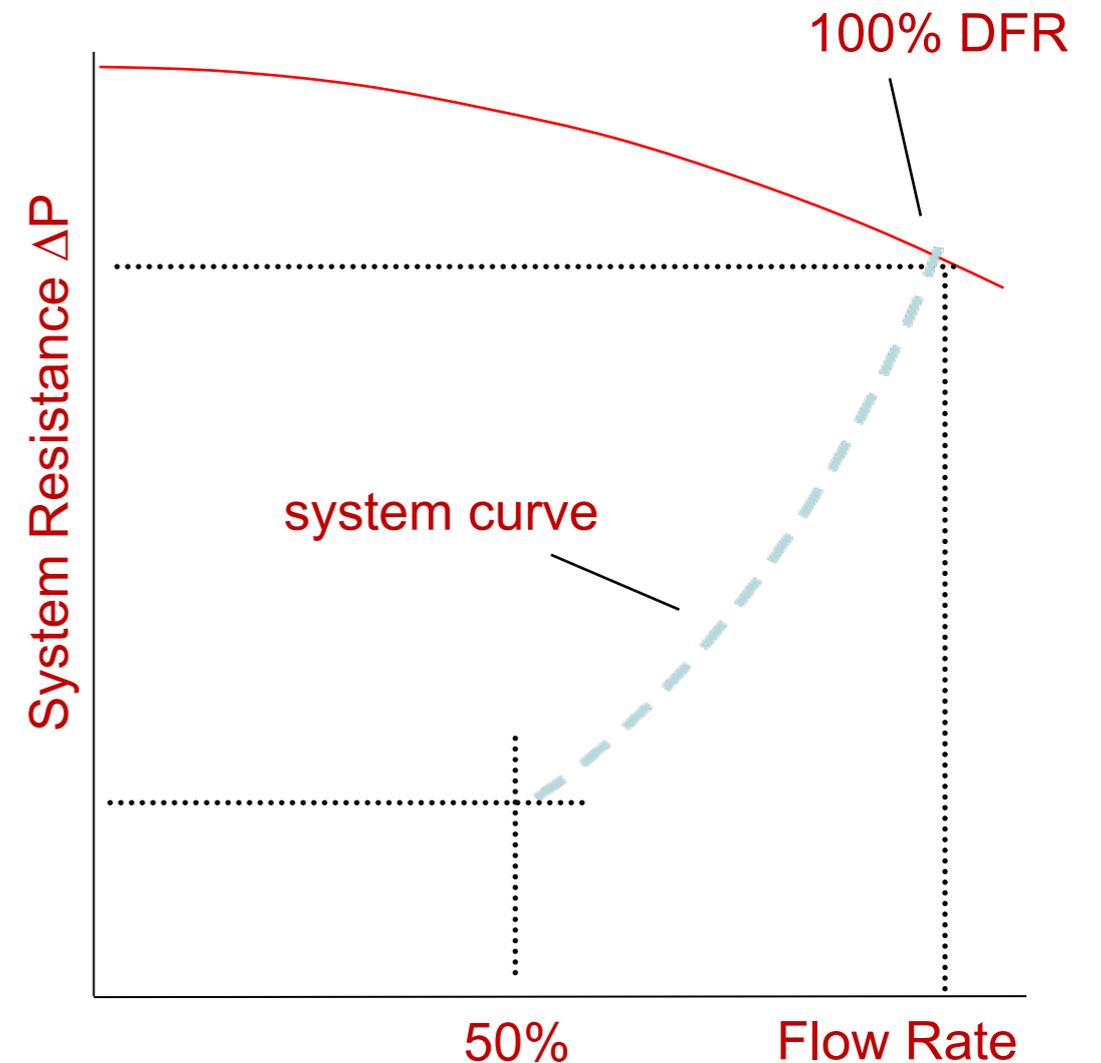
Temperature variations

- Over 70% of cooling season
- Load is less than 50%



Variable Volume Pump Energy Savings

- As system demand change, flow rate changes
- Direct relationship between pump speed and flow rate
- 50% pump speed = 50% flow rate



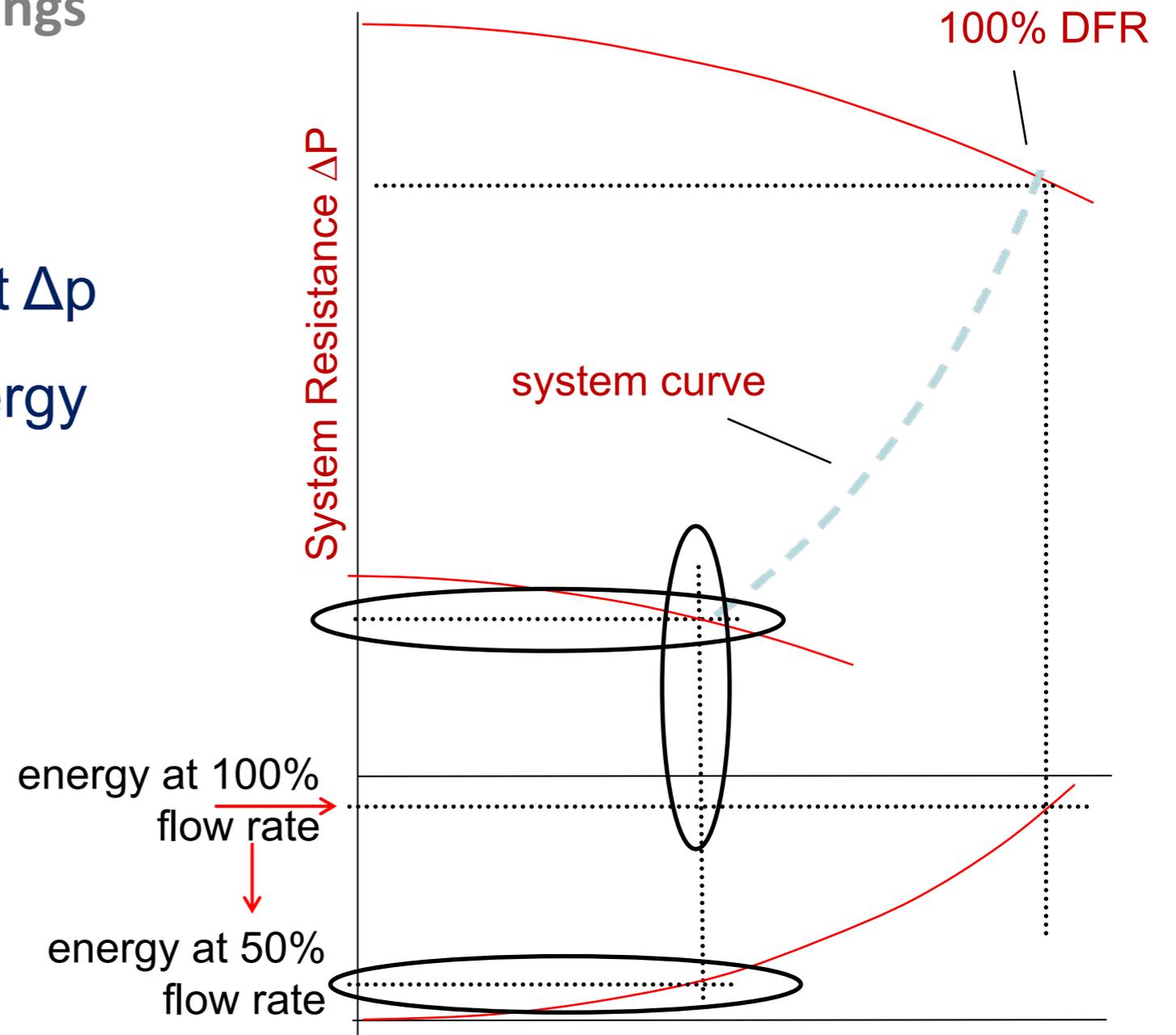
50% flow rate = 25% System Resistance

Variable Volume Pump Energy Savings

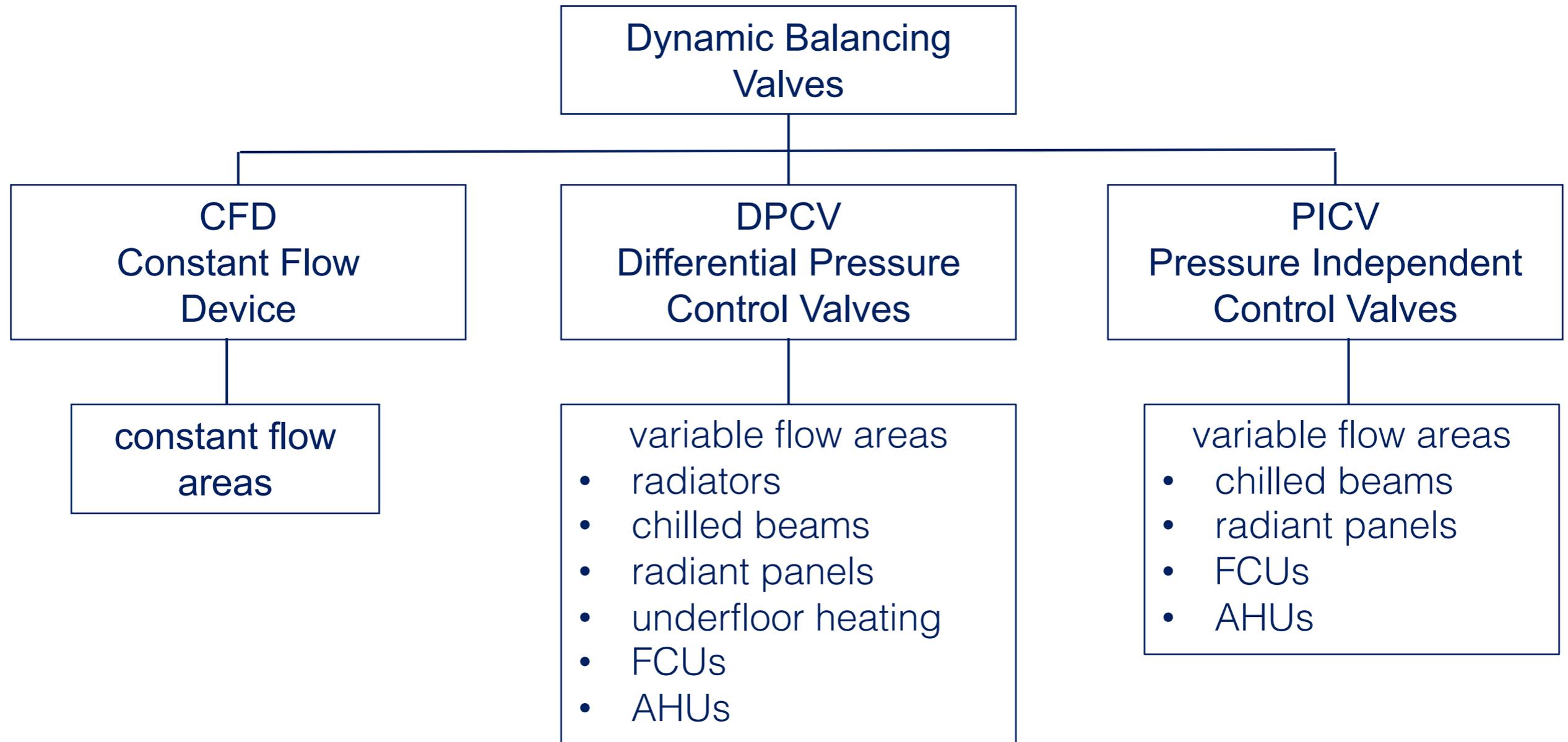
- 50% speed = 50% flow rate
- 50% flow rate = 25% circuit Δp
- 25% circuit Δp = 12.5% energy

*50% flow rate = over 70%
pump energy saving*

*Loses due to pump
efficiency reducing*



What are Dynamic Balancing Valves?

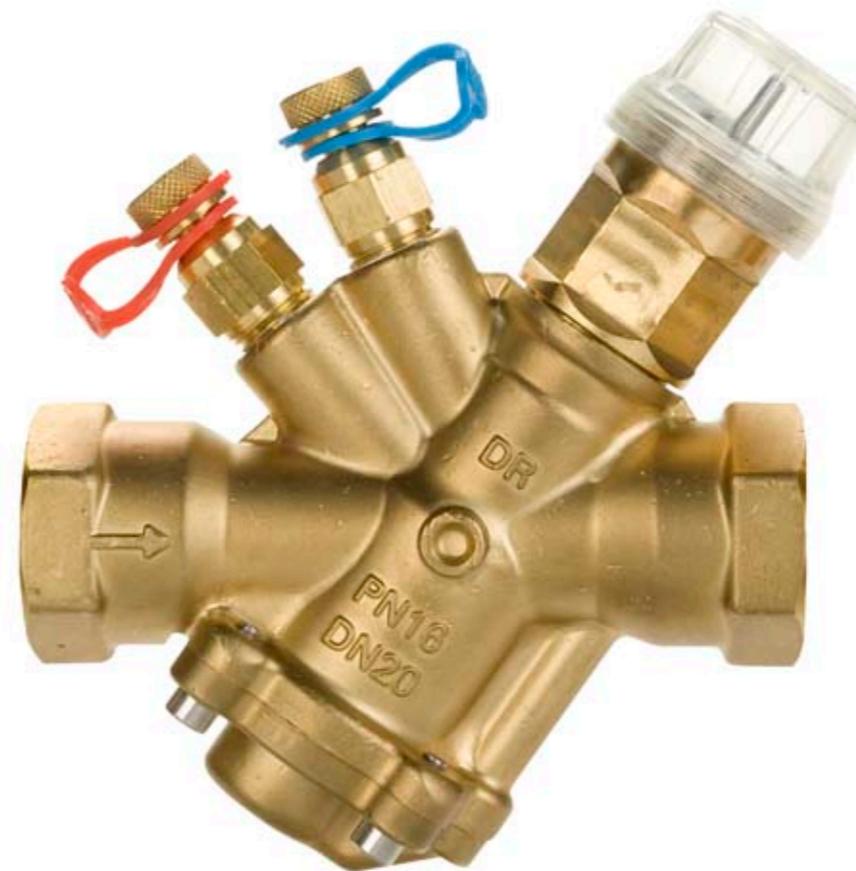


What are Dynamic Balancing Valves?

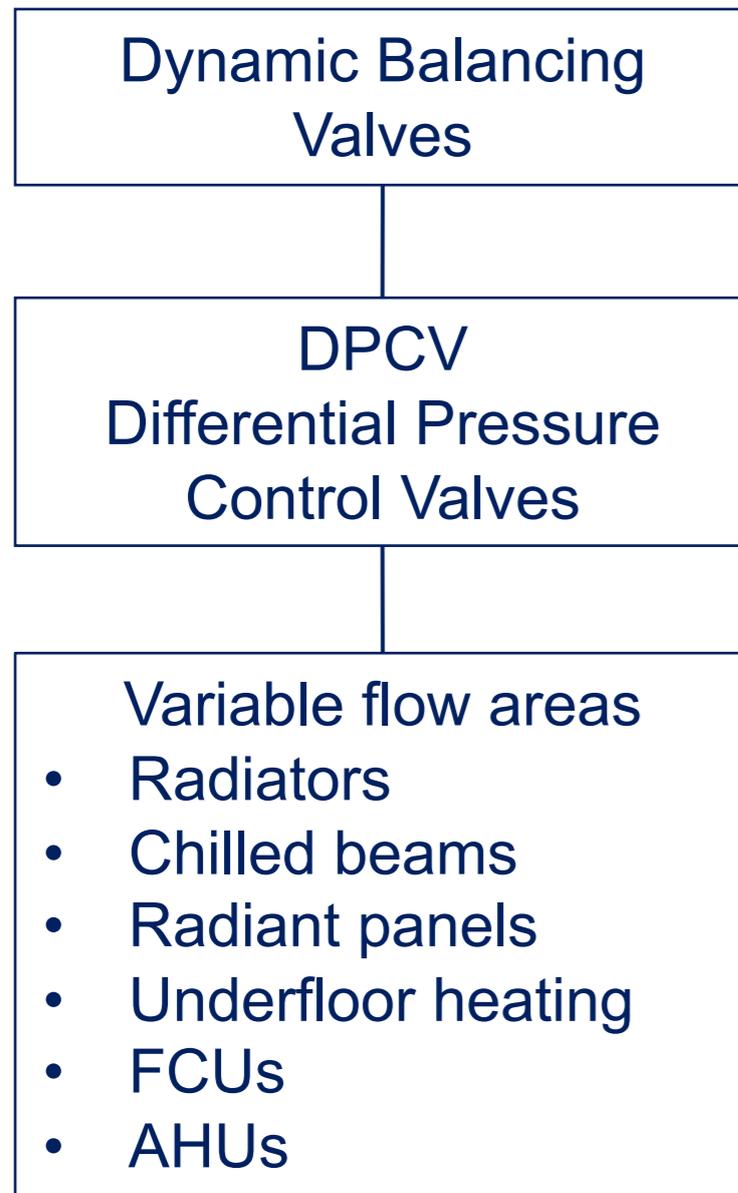
Dynamic Balancing
Valves

CFD
Constant Flow
Device

Constant flow
areas

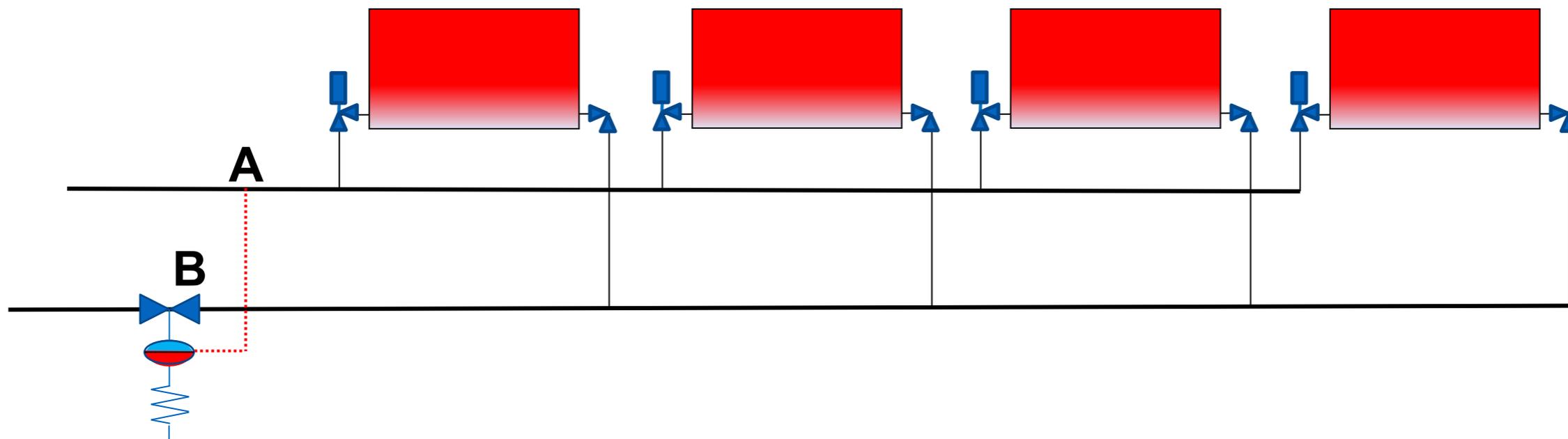


What are Dynamic Balancing Valves?



Why do we need Dynamic Balancing – radiator circuits

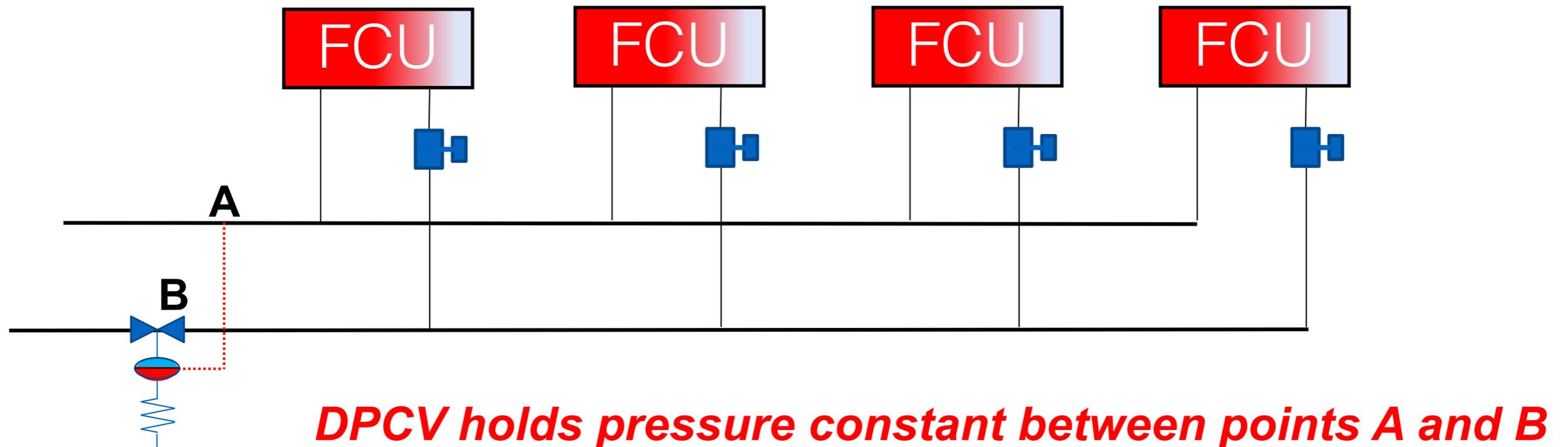
- To enable TRV (Thermostatic Radiator Valves) to correctly operate, a DPCV is installed to limit the radiator sub-circuit pressure differential
- The installation of DPCVs in sub-circuits with TRVs reduces the pressure that the TRV has to close against thus reducing the possibility of noisy valves



DPCV holds pressure constant between points A and B

Why do we need Dynamic Balancing – DPCVs for FCU

- To enable modulating 2 port control valves to operate with an acceptable authority, a DPCV is installed to limit the circuit pressure differential
- The installation of DPCVs on sub-branches with 2 port control valves is therefore essential to achieve good control



Why do we need DPCVs - control valve authority

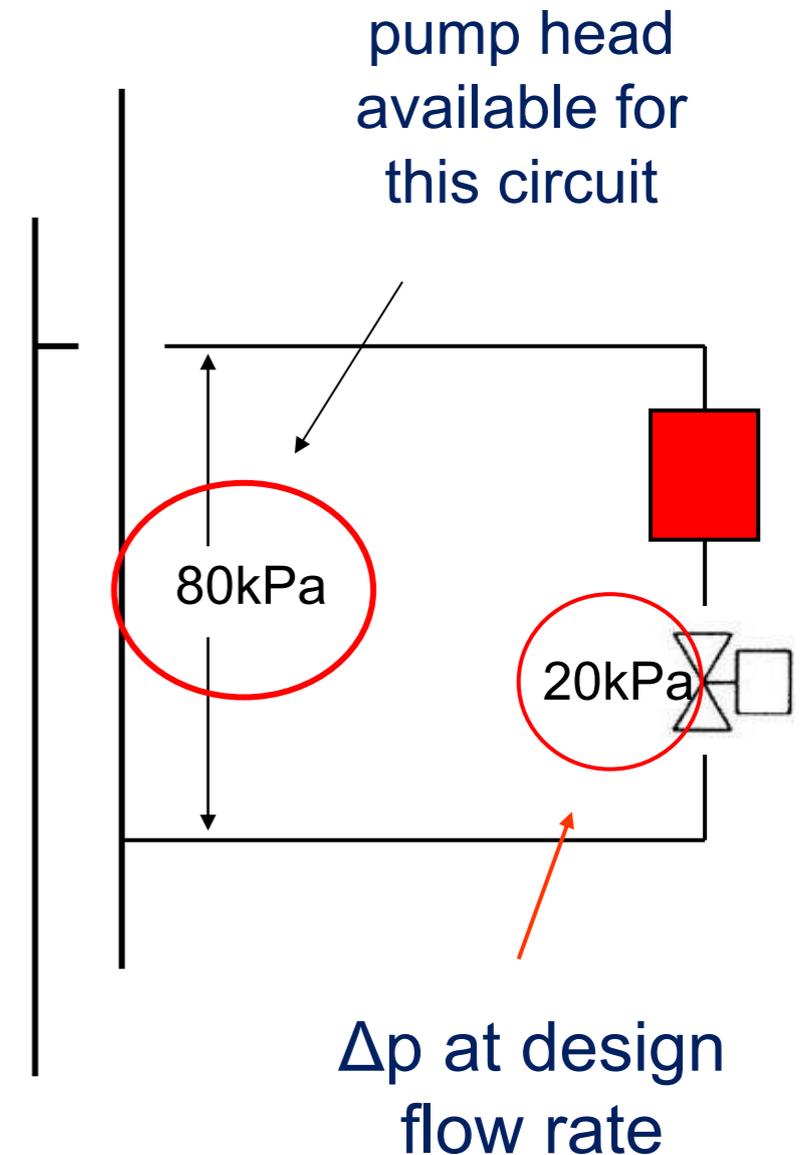
Example without DPCV

$$\text{valve authority } \beta = \frac{\Delta p \text{ across 2 port}}{\Delta p \text{ across circuit}}$$

$$\beta = \frac{20 \text{ kPa}}{80 \text{ kPa}}$$

$$\beta = 0.25$$

Too low - unacceptable



Why do we need DPCVs - control valve authority

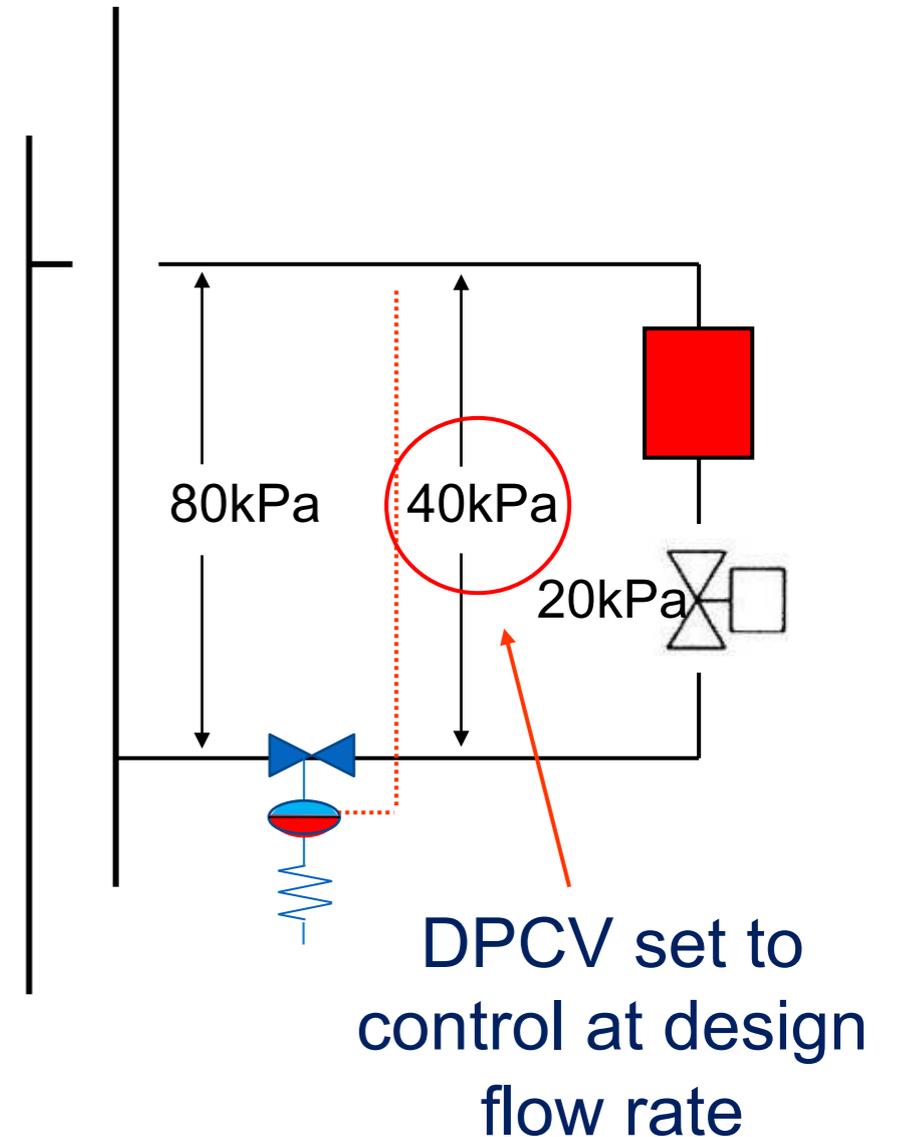
Example with DPCV fitted

$$\text{Valve authority } \beta = \frac{\Delta p \text{ across 2 port}}{\Delta p \text{ across circuit}}$$

$$\beta = \frac{20 \text{ kPa}}{40 \text{ kPa}}$$

$$\beta = 0.5$$

Acceptable



Why do we need DPCVs - control valve authority

Position of DPCV?

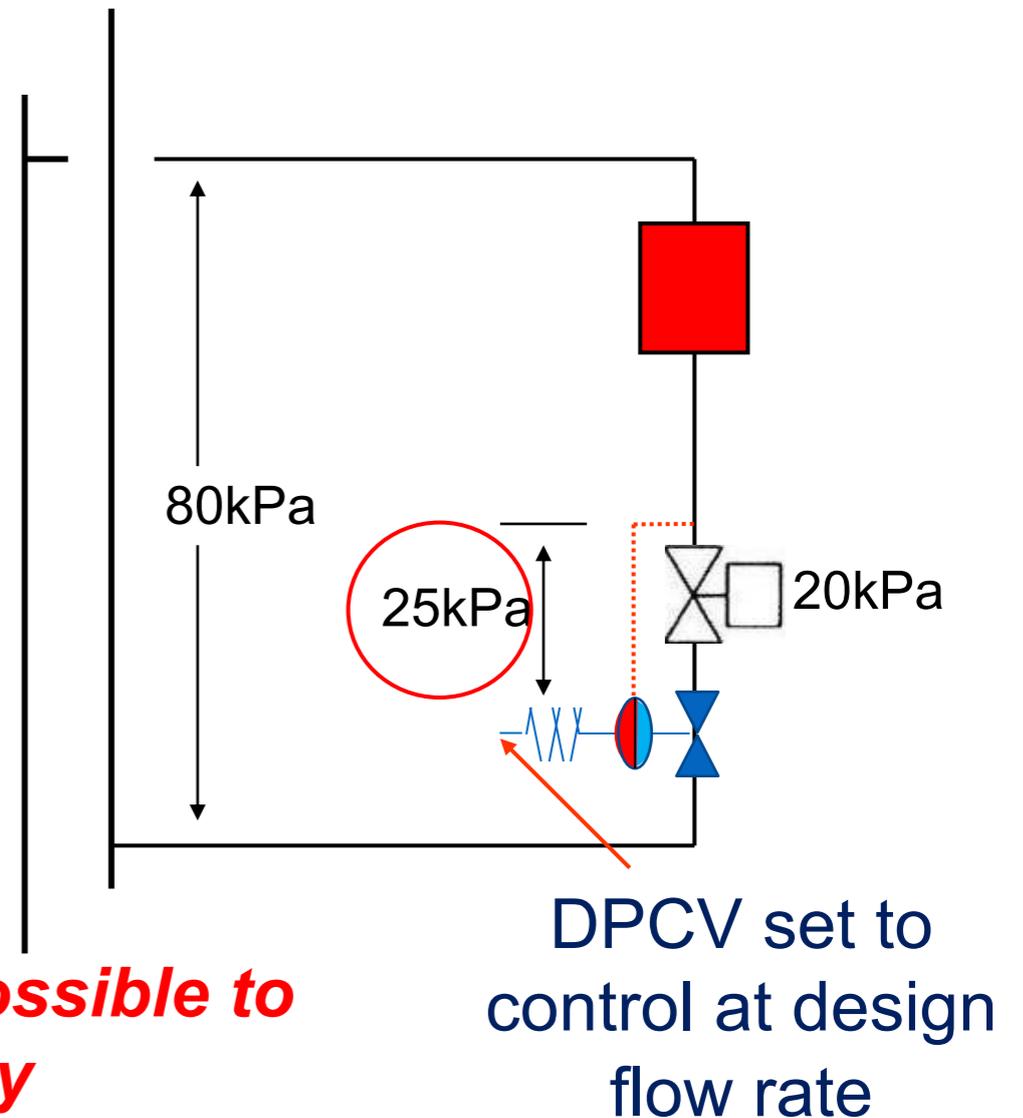
$$\text{valve authority } \beta = \frac{\Delta p \text{ across 2 port}}{\Delta p \text{ across circuit}}$$

$$\beta = \frac{20 \text{ kPa}}{25 \text{ kPa}}$$

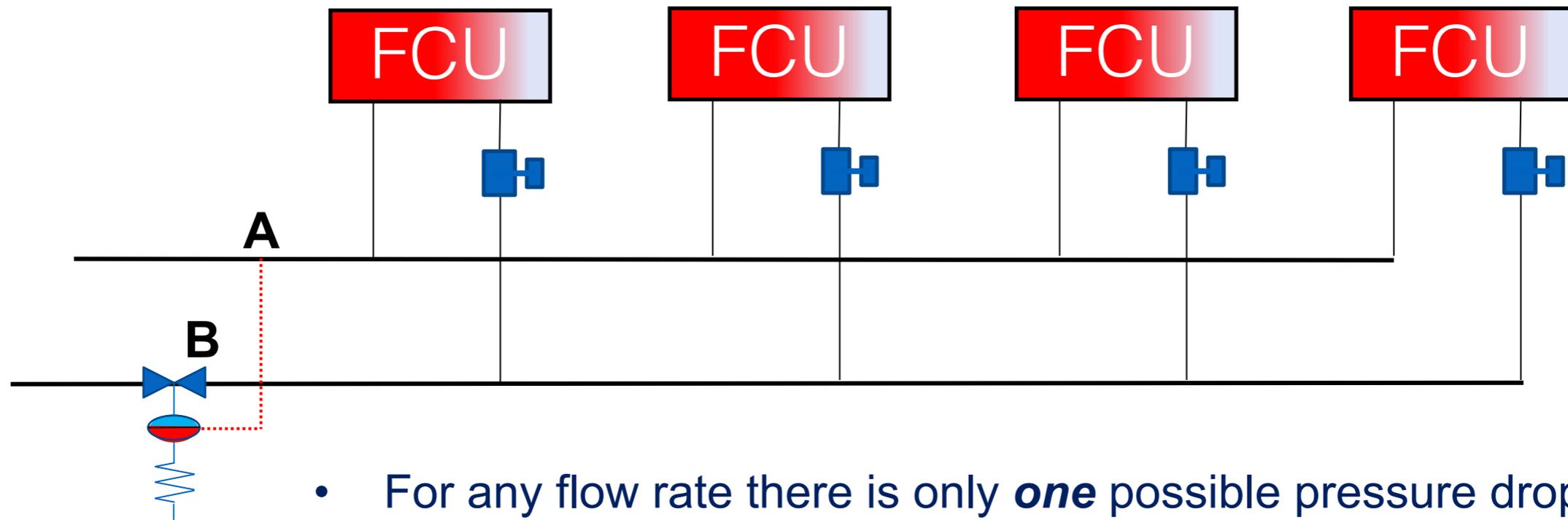
$$\beta = 0.8$$

position can influence authority

on single terminal circuits – as closes as possible to control valves gives higher authority



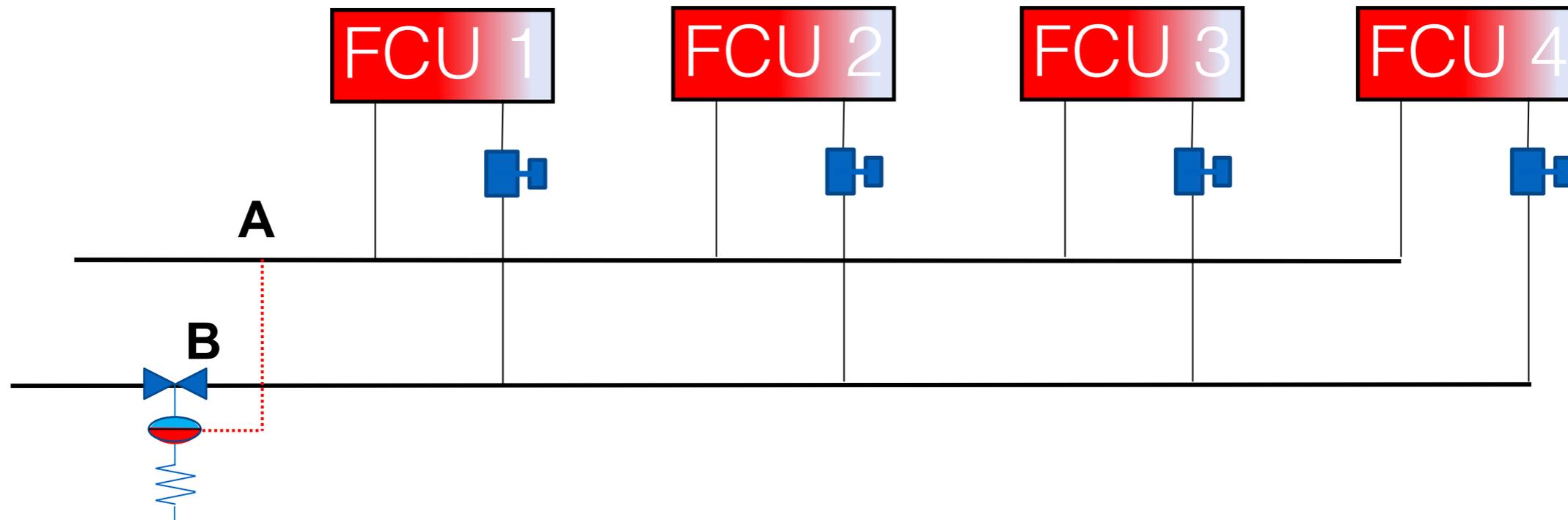
How do DPCVs work



- For any flow rate there is only **one** possible pressure drop between any 2 points
- As flow rate changes Δp changes – squared change
10% in flow = 21% in Δp

DPCV holds pressure constant between points A and B

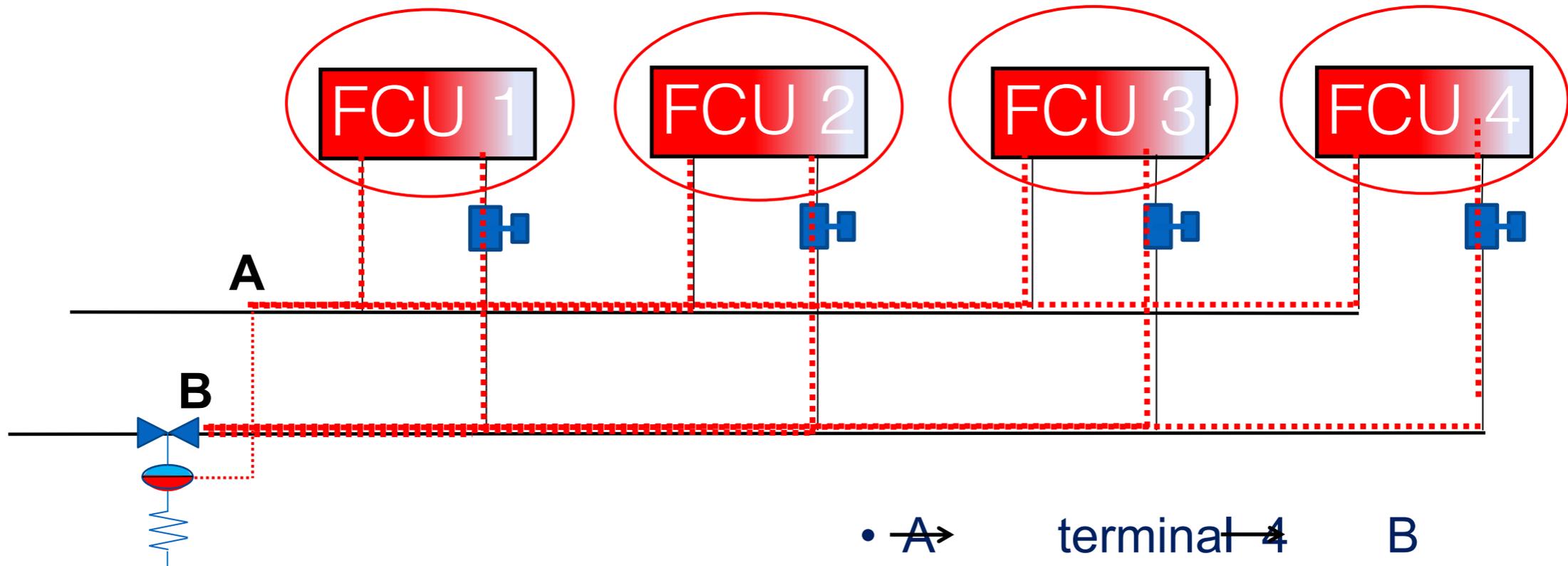
Why a DPCVs work



Kirchhoff's 2nd law states

'Head loss in parallel circuits must be equal'

Why a DPCVs work



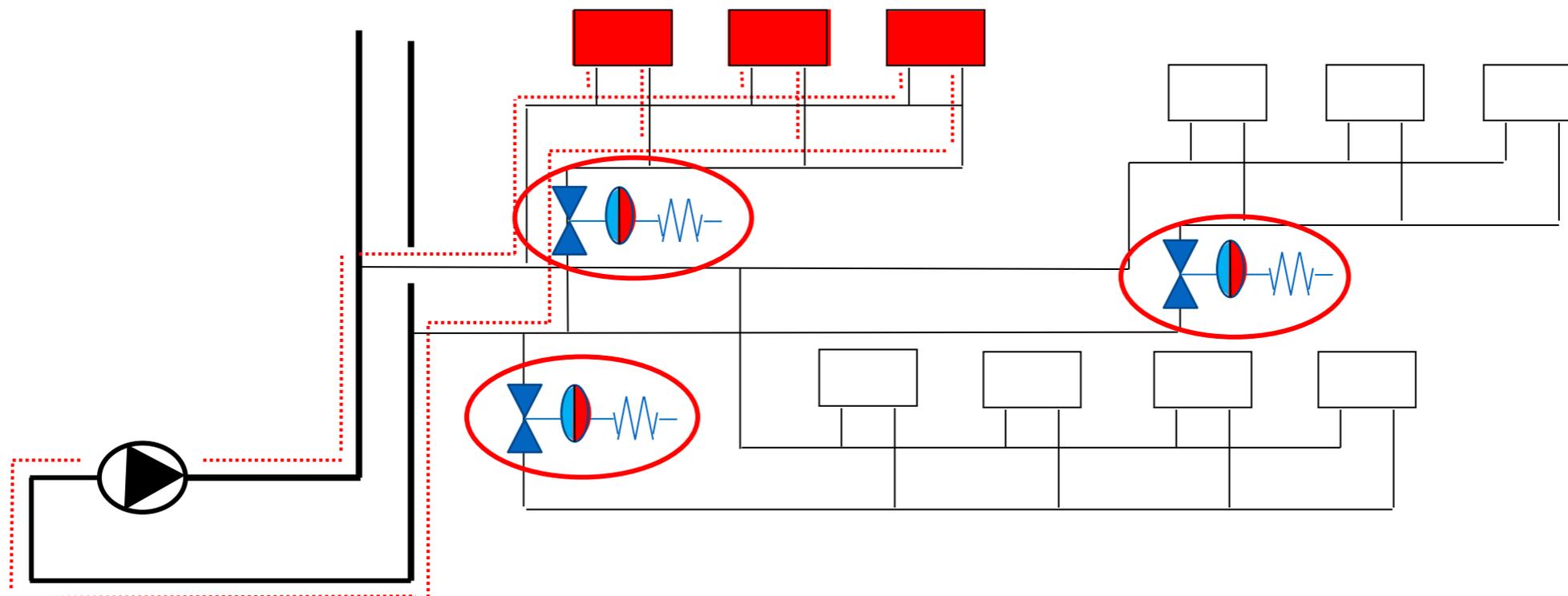
Applying Kirchhoff's law

- \overrightarrow{A} terminal \rightarrow 4 B
- \overrightarrow{A} terminal \rightarrow 3 B
- \overrightarrow{A} terminal \rightarrow 2 B
- \overrightarrow{A} terminal \rightarrow 1 B

All have the same pressure drop irrespective of flow

Where do DPCVs go

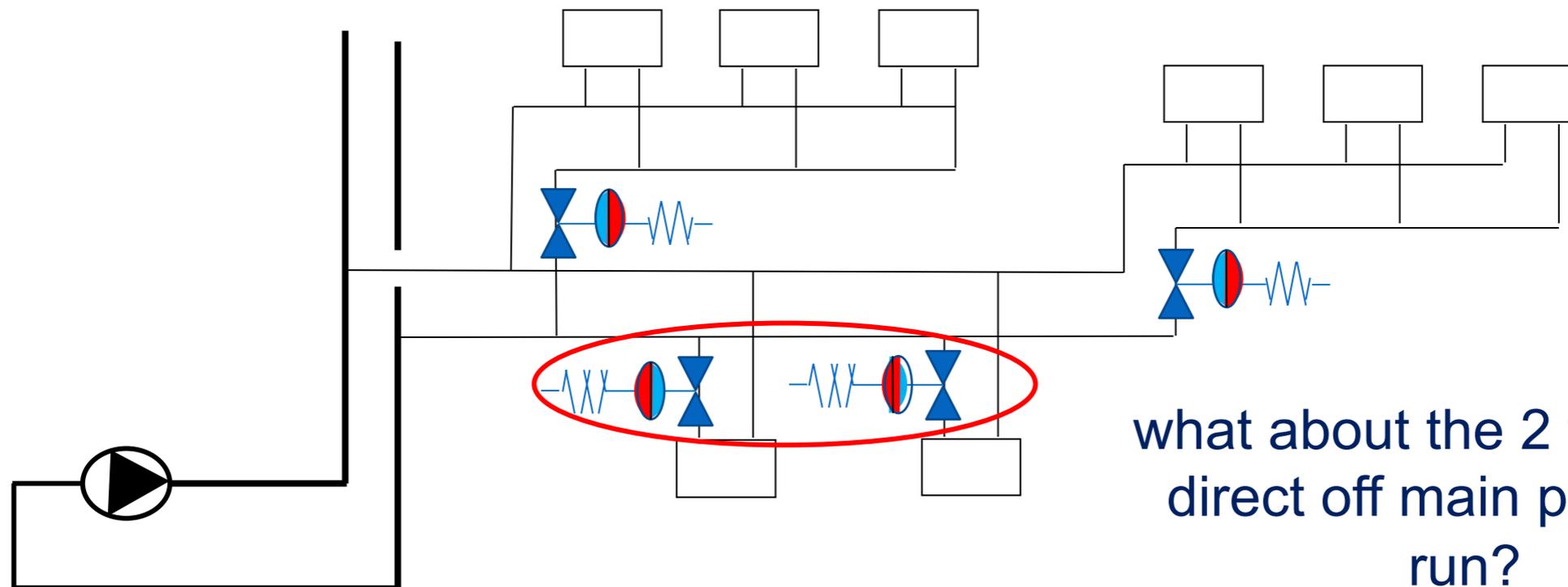
Branches are broken down into sub-circuits, each controlled by a DPCV



Each circuit must only flow through a single DPCV

Where do DPCVs go

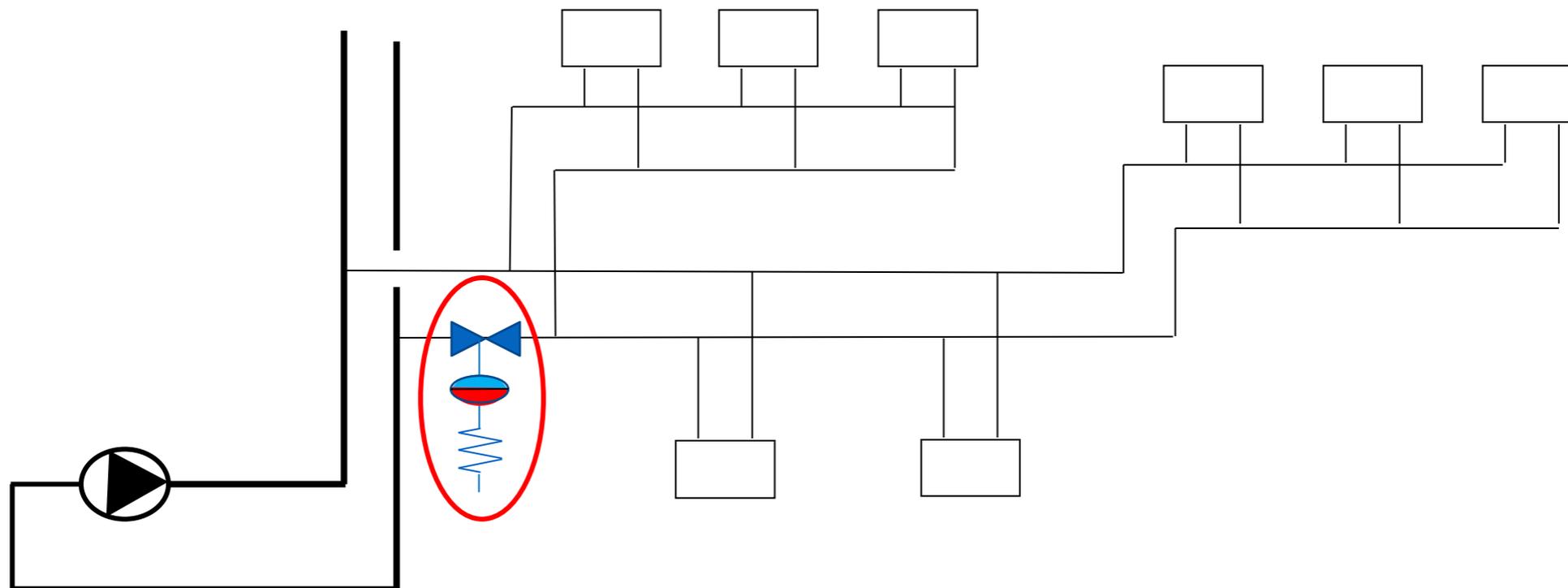
Branches are broken down into sub-circuits, each controlled by a DPCV



Each circuit must have some protected from over flow

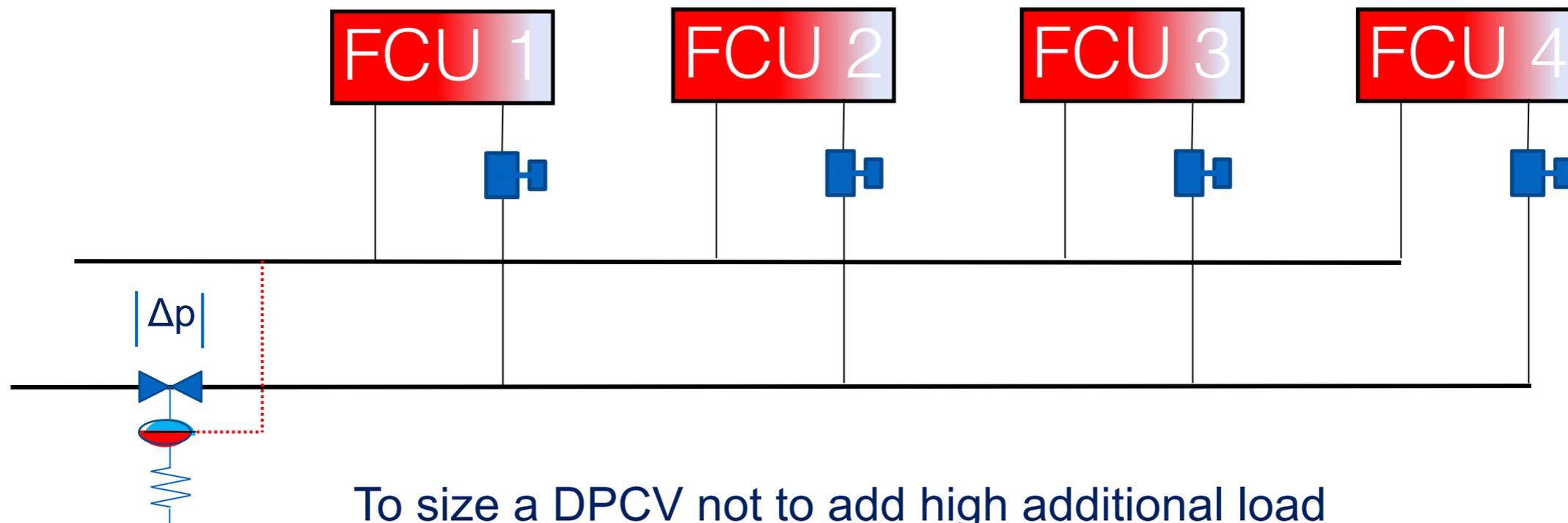
Where do DPCVs go

Alternative approach



Complete circuit protected by a single DPCV

How are DPCVs selected



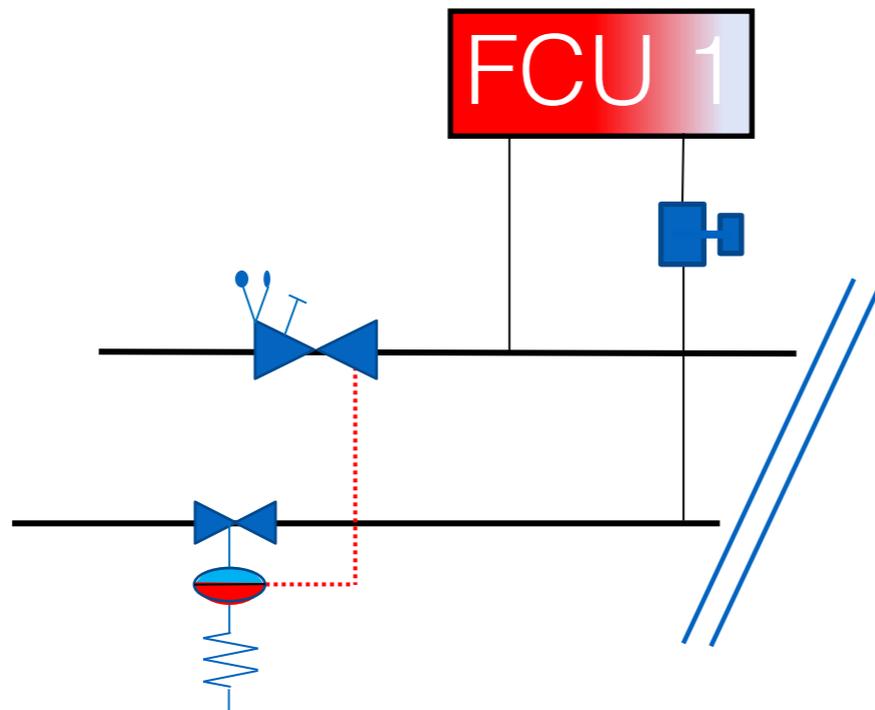
To size a DPCV not to add high additional load

the Δp across the DPCV

is typically 10 - 20kPa

irrespective of the Δp through the circuit

Other Valves associated with DPCVs - Companion Valve



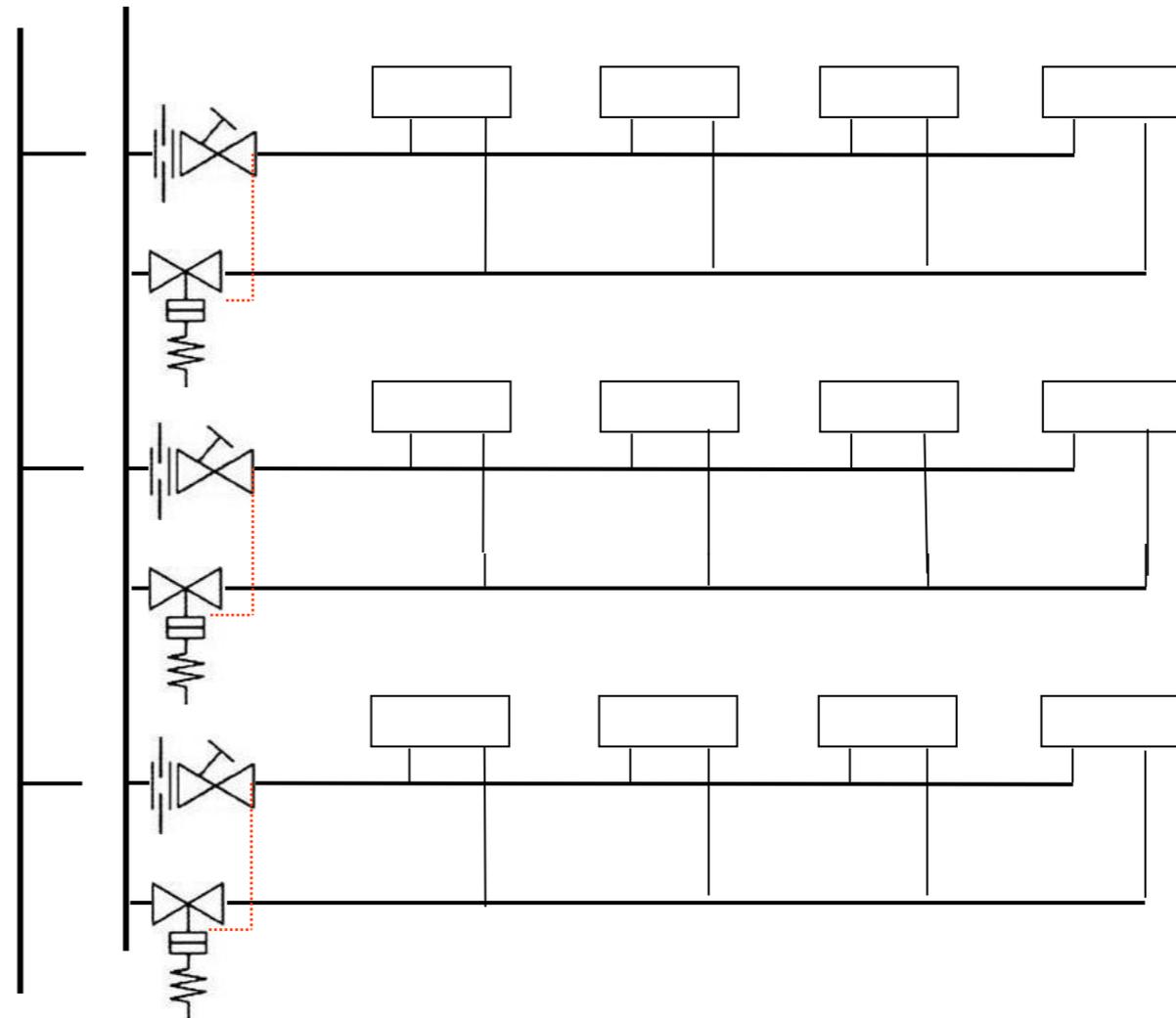
Companion Valve offers

- flow measurement
- isolation
- DPCV connection
- bosses for test points



Dynamic Balancing of the System

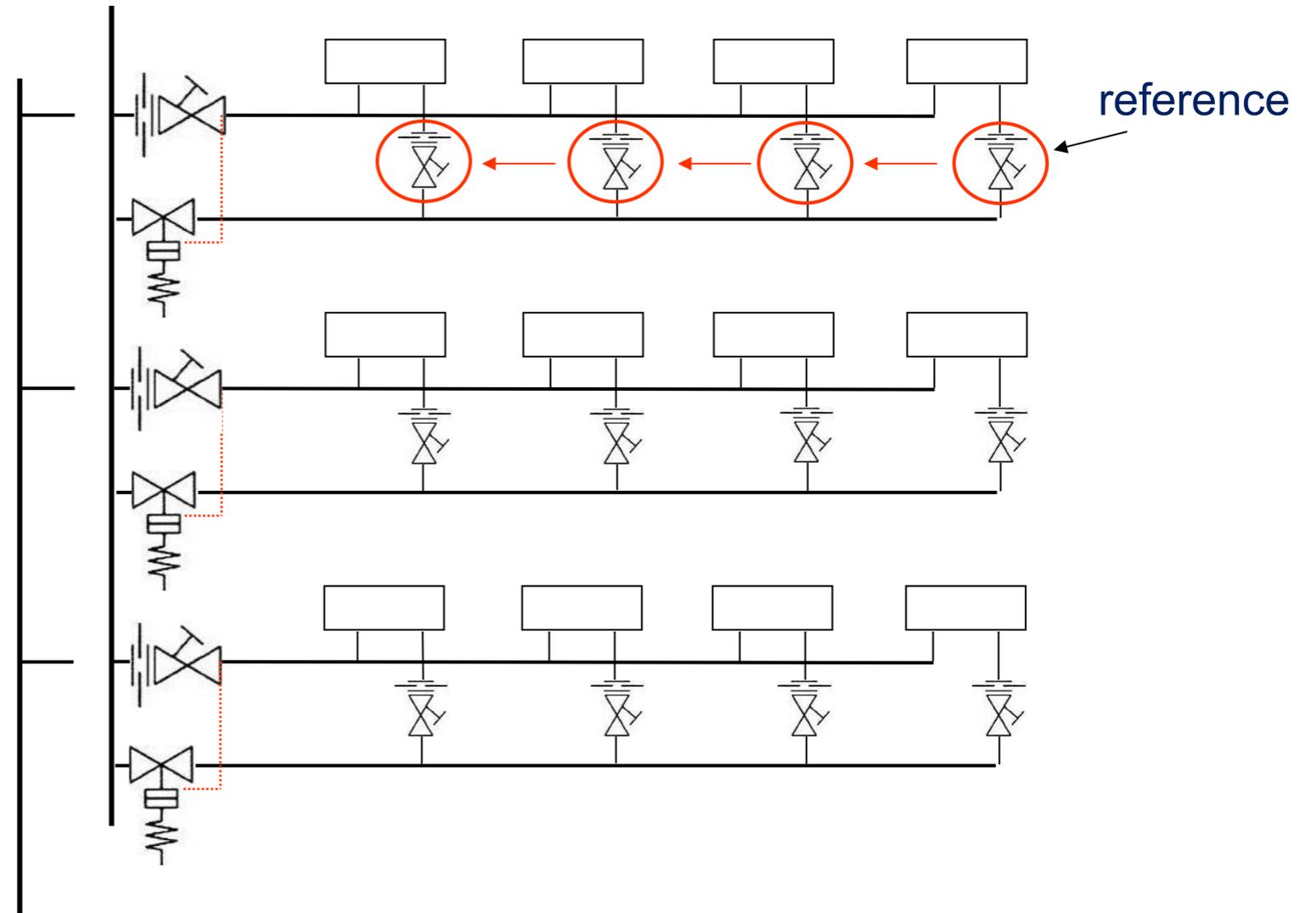
Because each sub-circuit is separated by a DPCV from fluctuating system pressure & therefore holds a constant pressure within the sub-circuit, commissioning sub-circuits can be carried out totally independently



sub-circuits are independent of each other

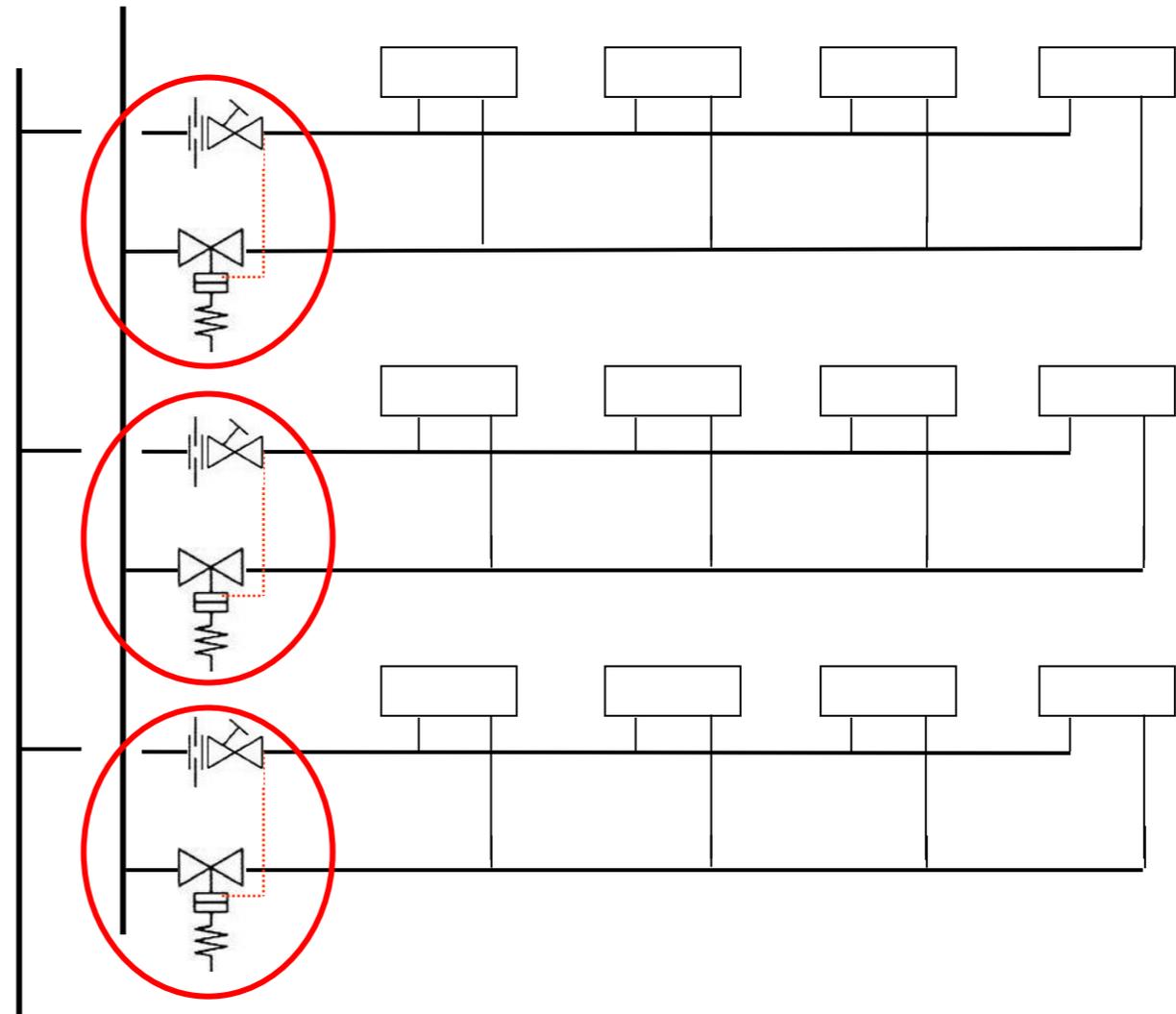
Dynamic Balancing of the System

Commissioning within the sub-circuits is carried out by 'proportional balancing' in the conventional manner



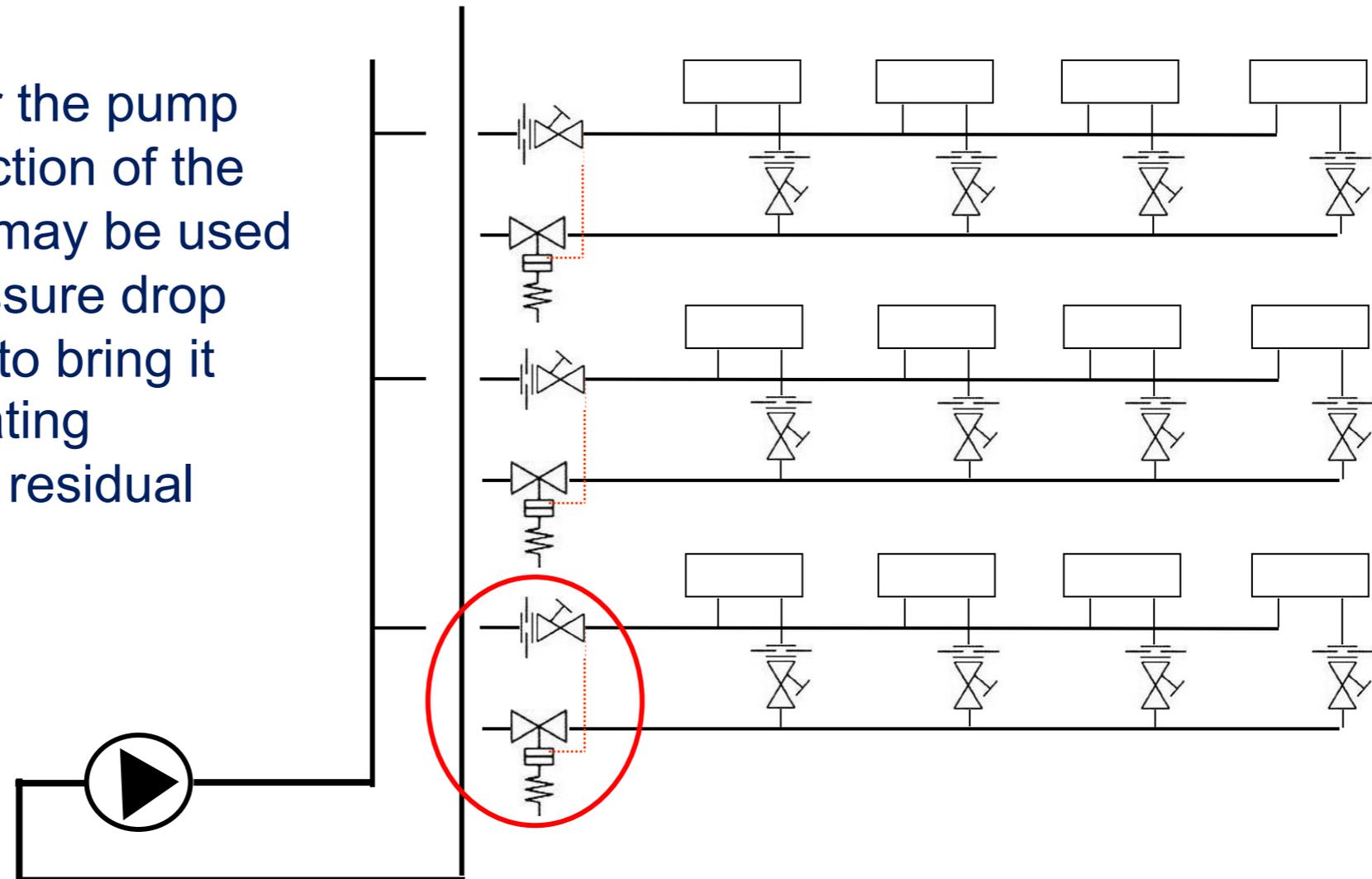
Dynamic Balancing of the System

Each sub-circuit is balanced by measuring flow thro the 'Companion Valve' and adjusting DPCV to regulate flow

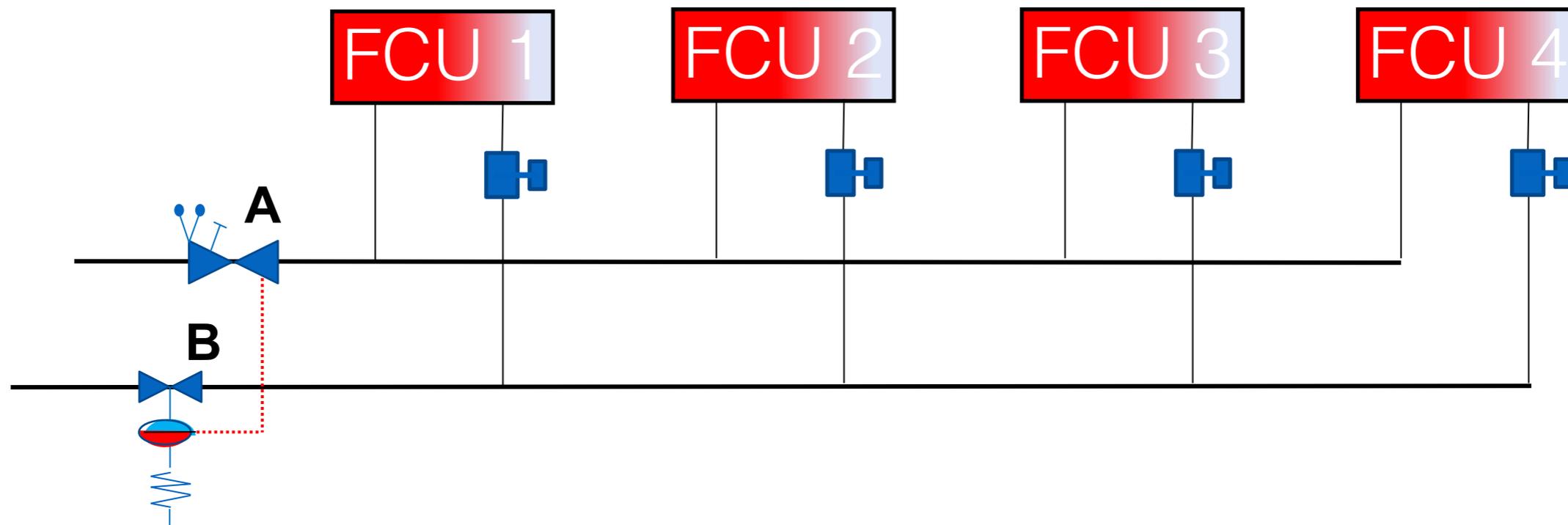


Dynamic Balancing of the System

For circuits nearer the pump the regulating function of the companion valve may be used to reduce the pressure drop across the DPCV to bring it into a better operating position, i.e. splits residual pressure



Dynamic Balancing of the System



1. set DPCV to highest control range setting
 - highest pressure difference gives highest flow rates
2. measure flow rate at companion valve
3. adjust DPCV until design flow rate achieved

Variable Volume System

At maximum pump turndown, typically 10 - 20%, consideration needs to be given to branches to ensure

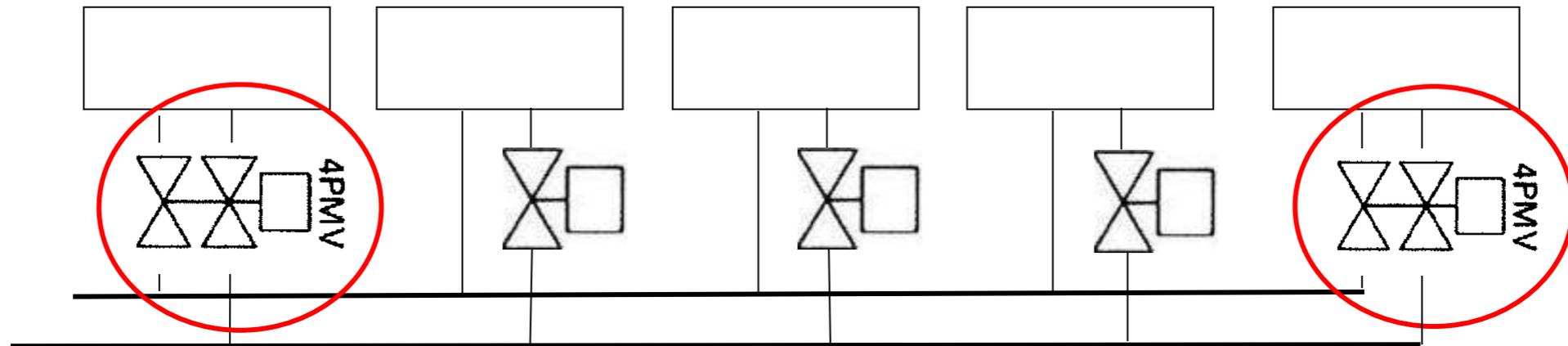
- pump flow at minimum load
- circulation of water treatment
- ready supply of heating / chilled water

Dynamic Balancing of the System

possible solution

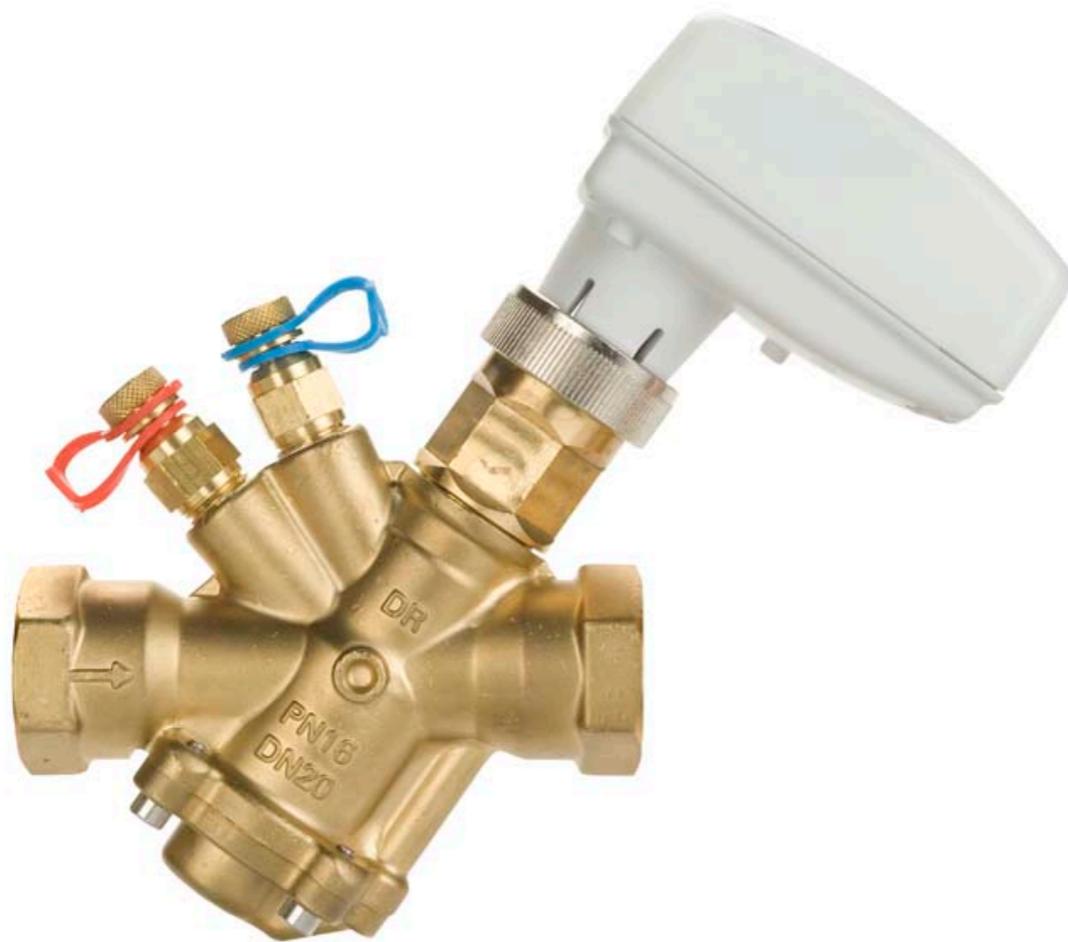
end terminal could have a 3 or 4 port control valve

- on larger circuits additional 3 or 4 ports could be added



What are Dynamic Balancing Valves?

Dynamic Balancing
Valves



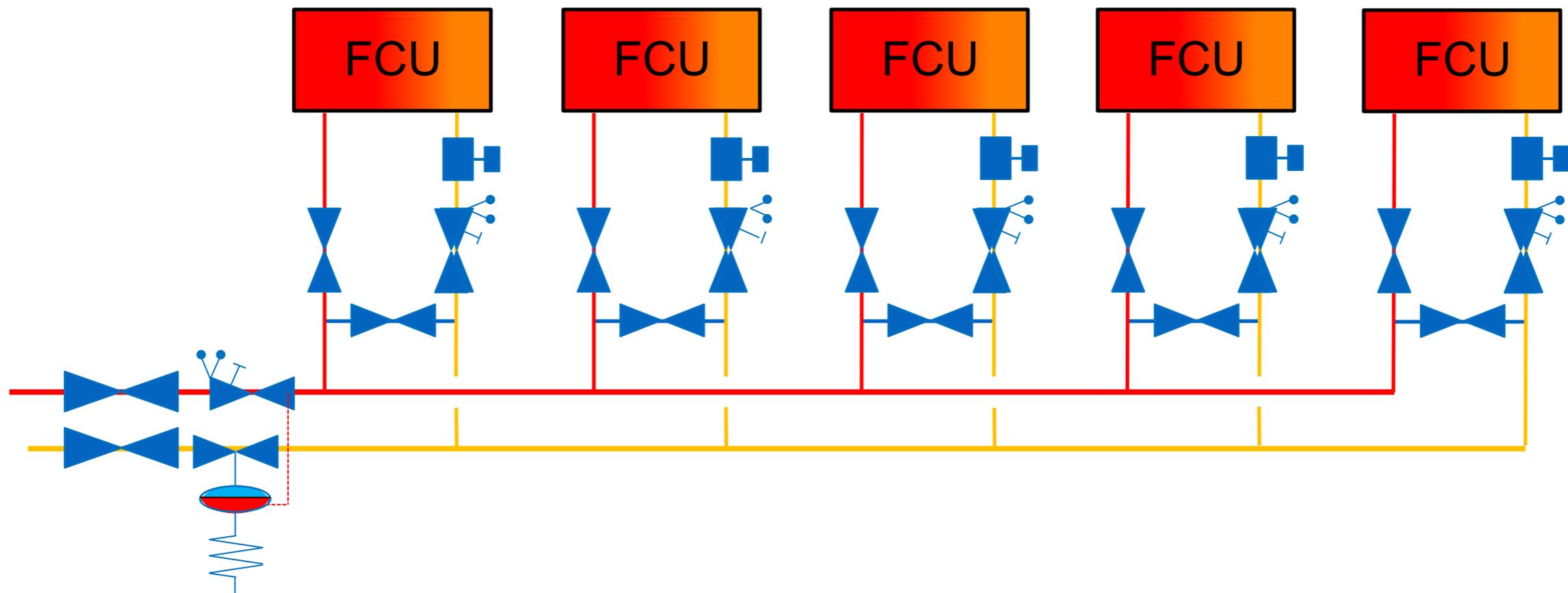
PICV
Pressure Independent
Control Valves

- Variable Flow Areas**
- chilled beams
 - radiant panels
 - FCUs
 - AHUs

Controlling Fluctuating System Pressures

Following the move to *variable volume* system design

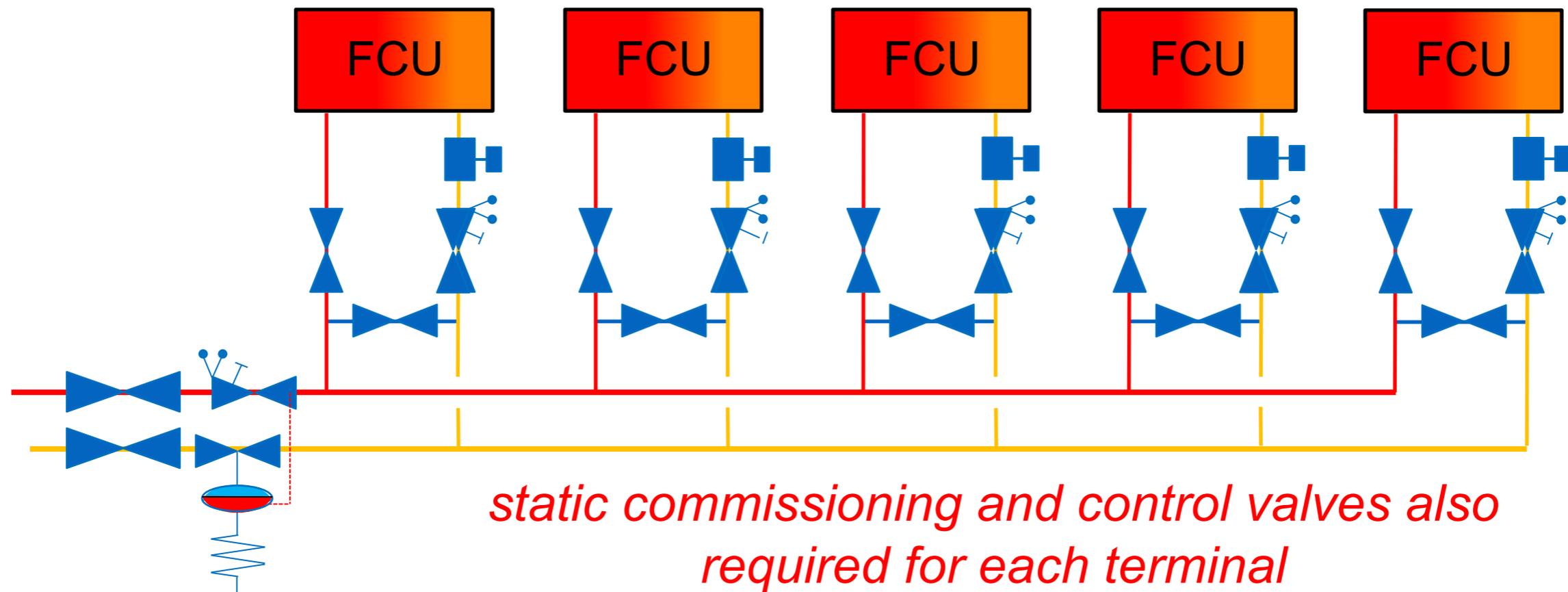
- DPCVs were used to create areas with stable pressures



Controlling Fluctuating System Pressures

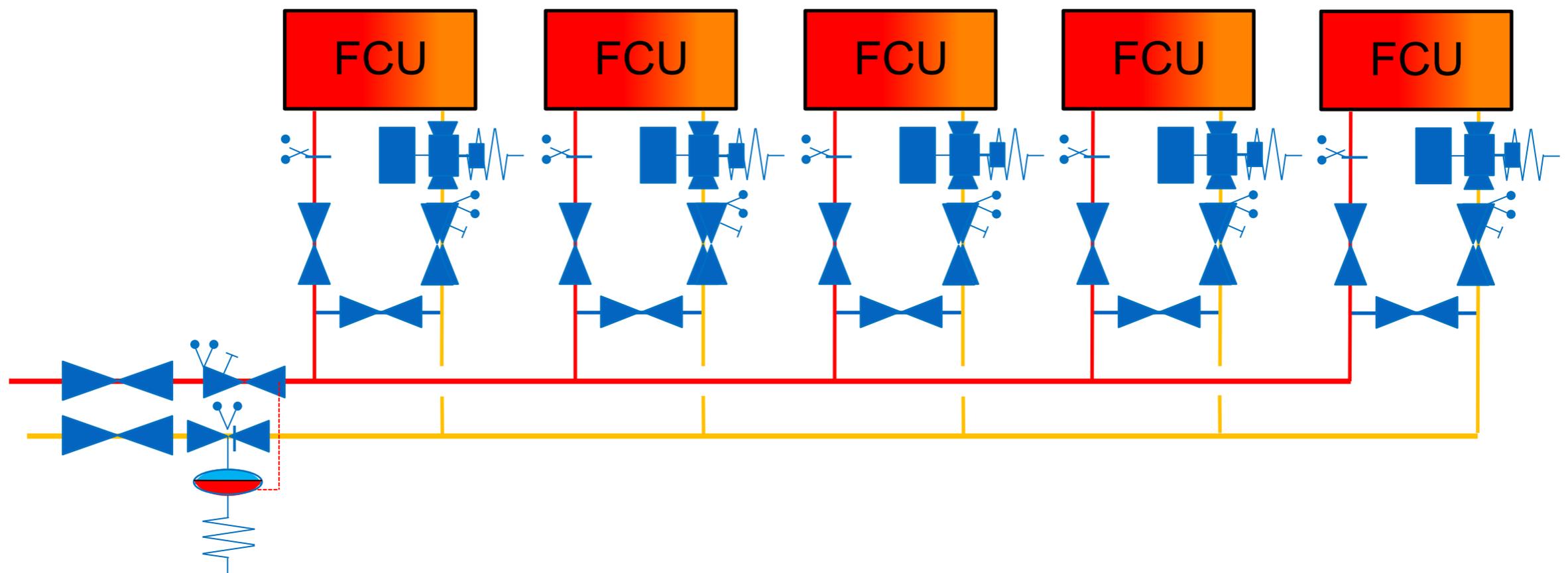
DPCVs prove difficult to select correctly

- sizing relatively easy
- gathering required information difficult / impossible
 - number of terminals in protected zone / controlled D_p ?



Controlling Fluctuating System Pressures

PICVs replacing DPCVs
other valves required?

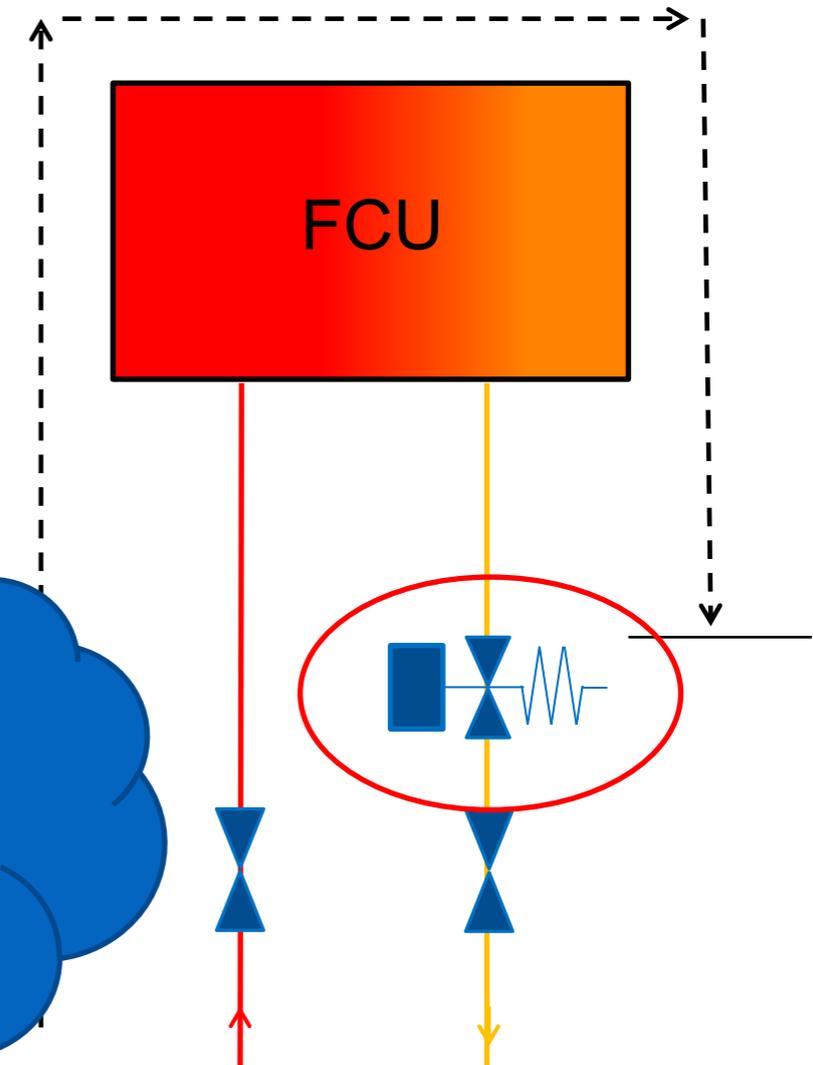


the PICV is fitted instead of – not as well as

Controlling Fluctuating System Pressures

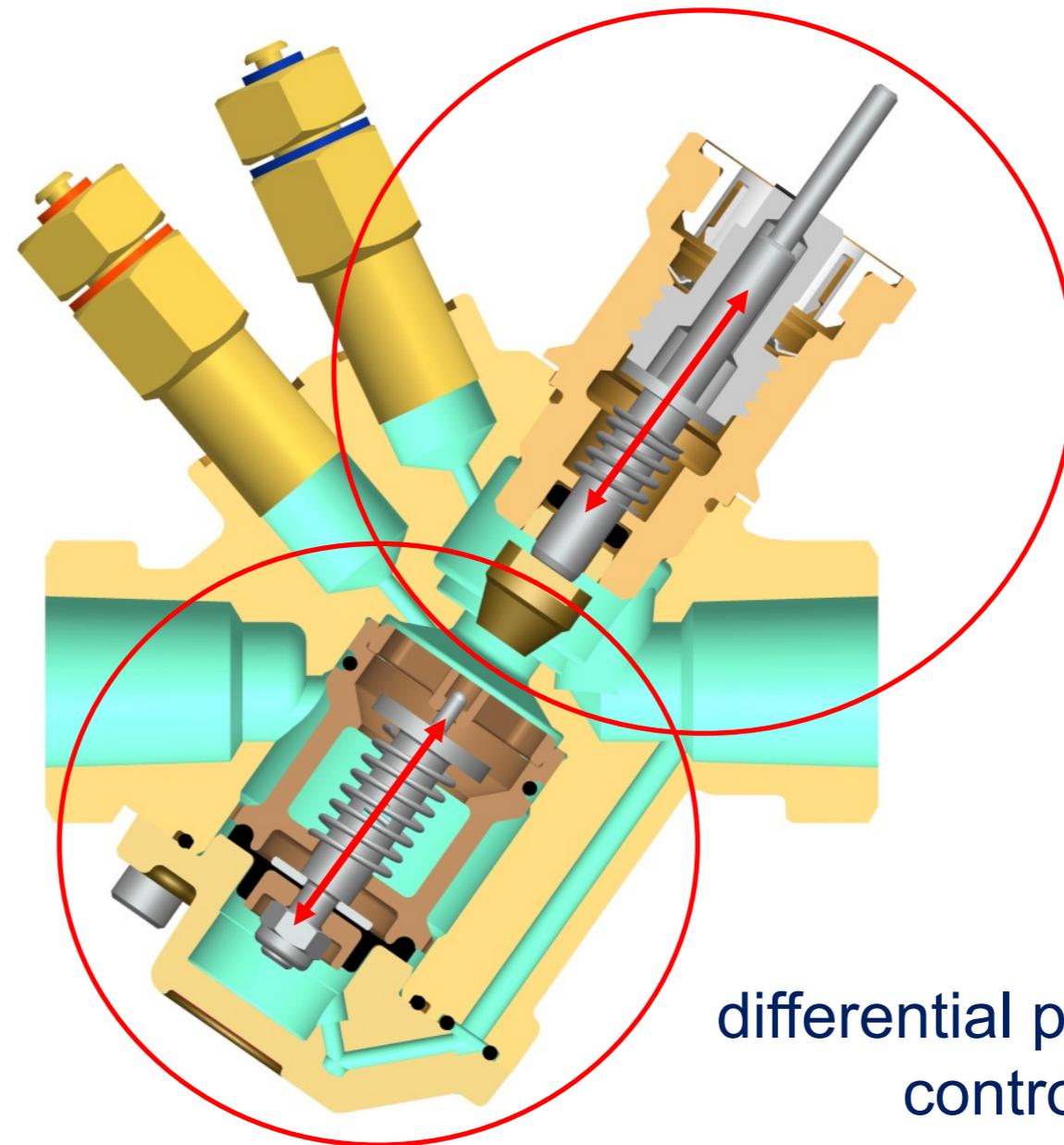
- Normally fitted to each terminal unit
- Return pipework is the preferred position
- Clear / straight lengths of pipework are *not* required for PICVs but 'good practice' suggests some straight lengths of pipework create a more stable flow pattern for the PICV to control

coil kept in highest pressure available



What is a PICV?

Three functions in one



flow regulation

flow control

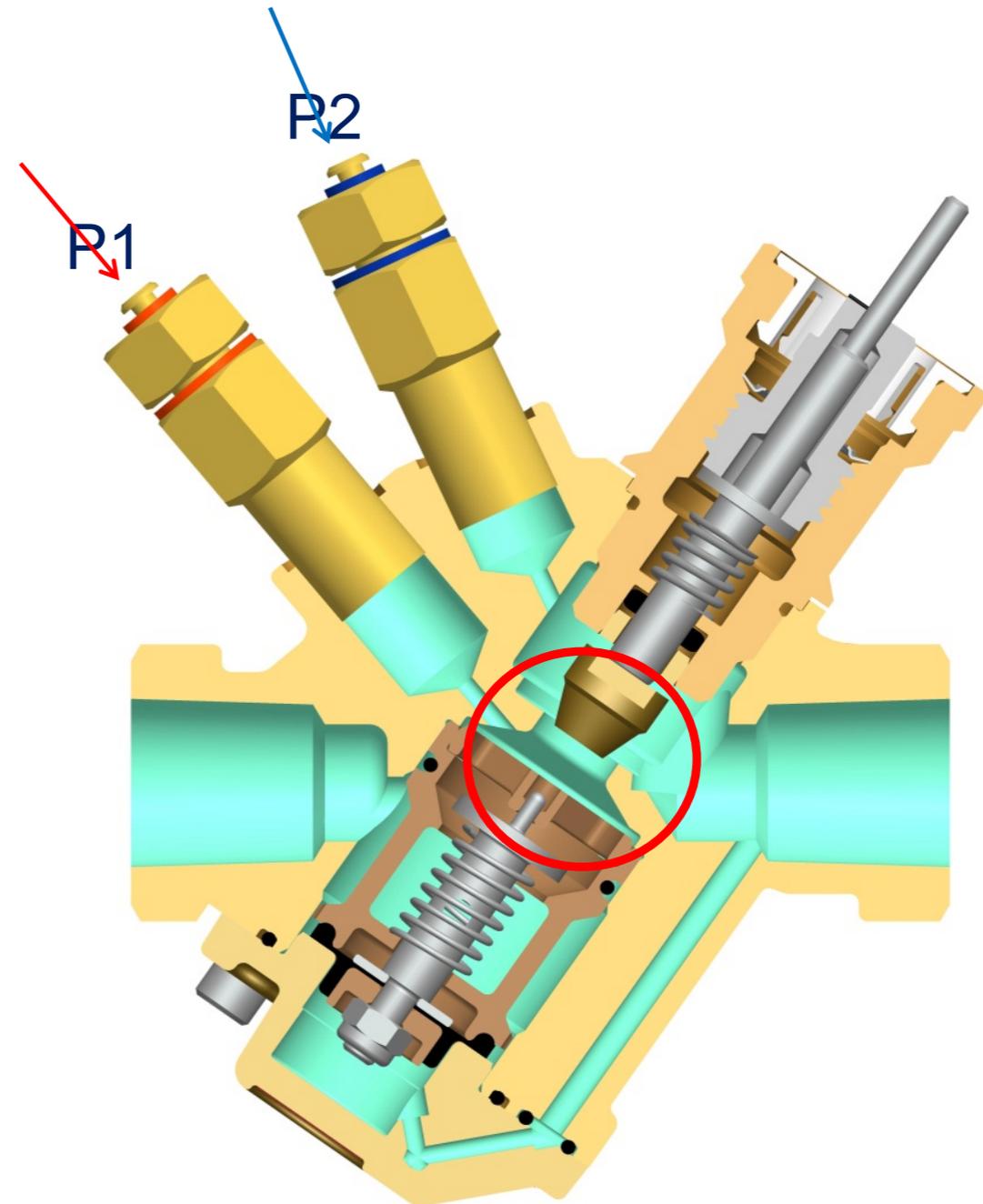
differential pressure control

Pressure Drops Across PICV

Differential pressure controller holds the Dp across the seat constant

Dp confirmed by test points

Often referred to as P1 – P2

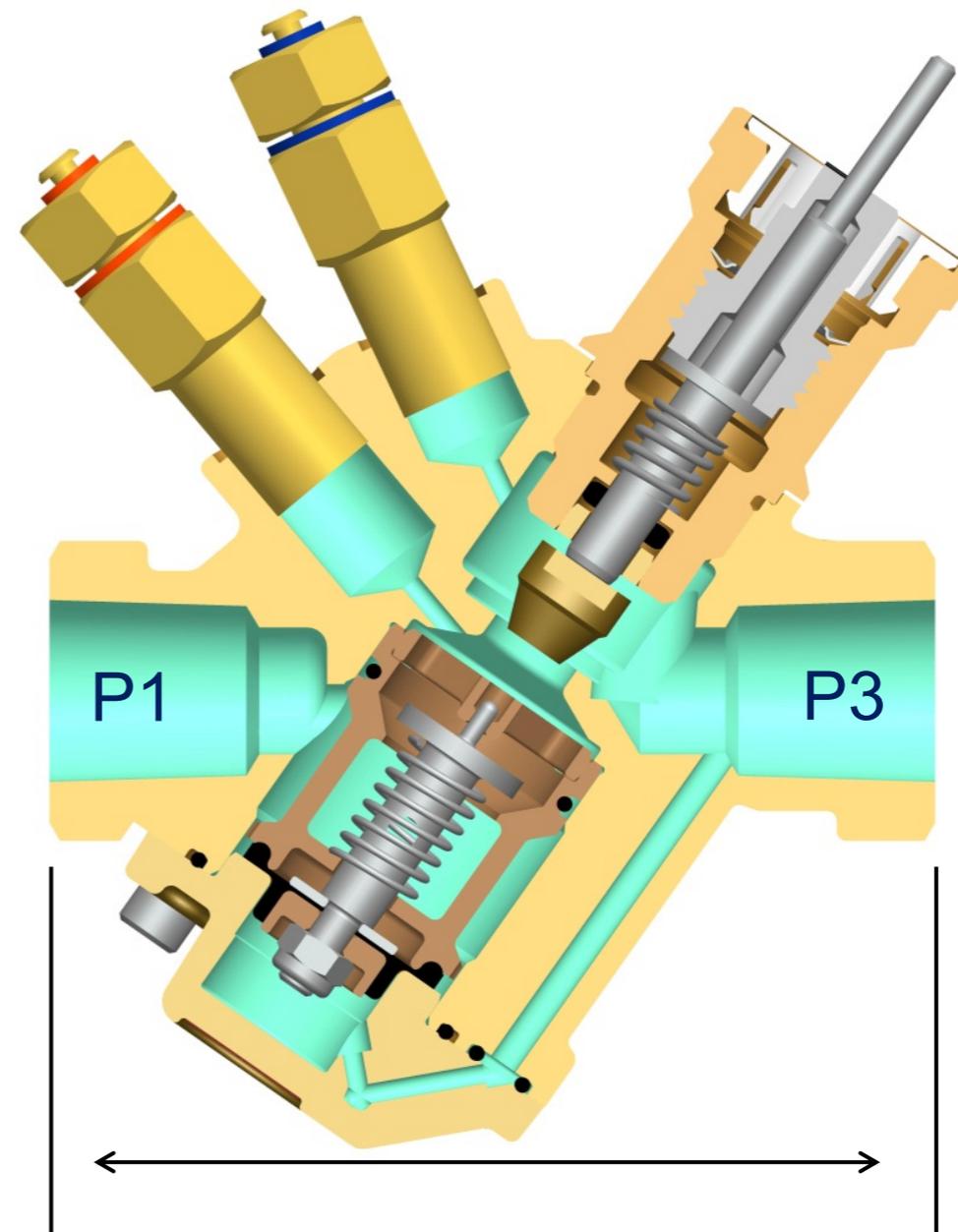


Pressure Drops Across PICV

Differential pressure
across the PICV
varies

On smaller sizes
total Dp
NOT
confirmed by test
points

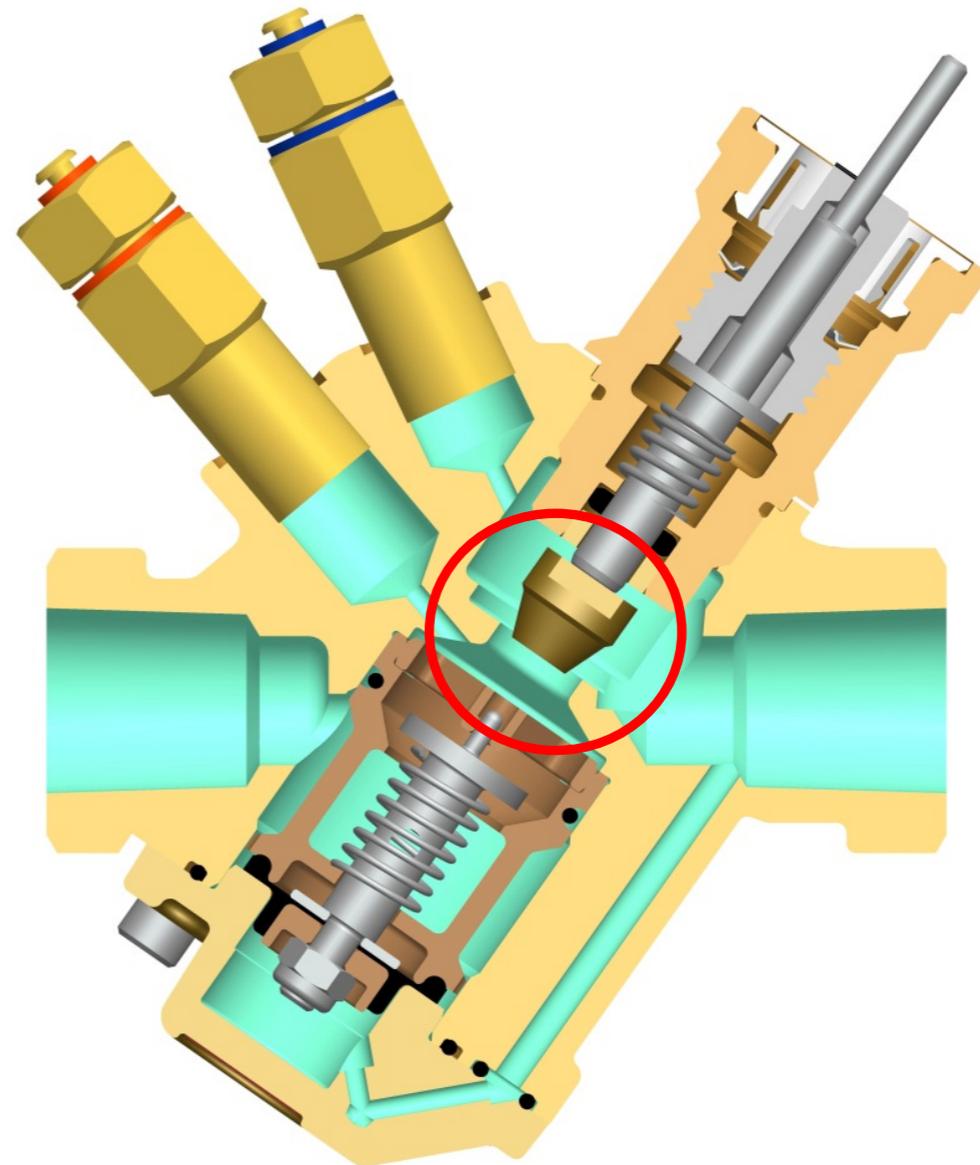
*Often referred to
as P1 – P3*



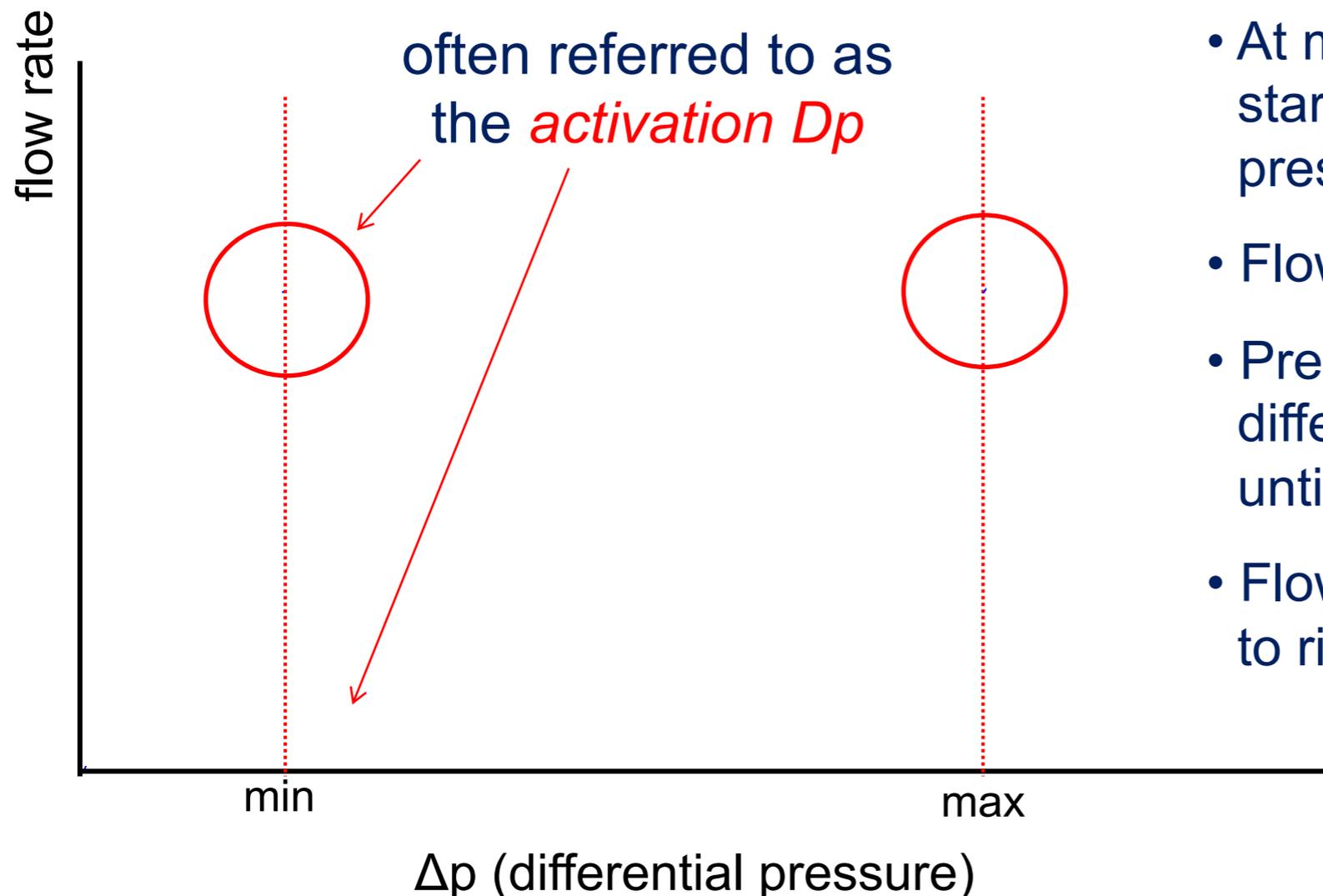
$$\text{Authority } h = \frac{\text{Dp across control valve}}{\text{DP across circuit}}$$

$$\text{Dp control valve} = \text{DP circuit}$$

Considered to be '1'



PICV Activation



- As flow increases Δp increases
- At min Δp , pressure controller starts to hold differential seat pressure constant
- Flow rate remains constant
- Pressure controller controls seat differential pressure at *min Δp* until *max total Δp* is reached
- Flow rate will rise as Δp continues to rise

PICV Activation

P1 to P2

the activation Δp

always constant

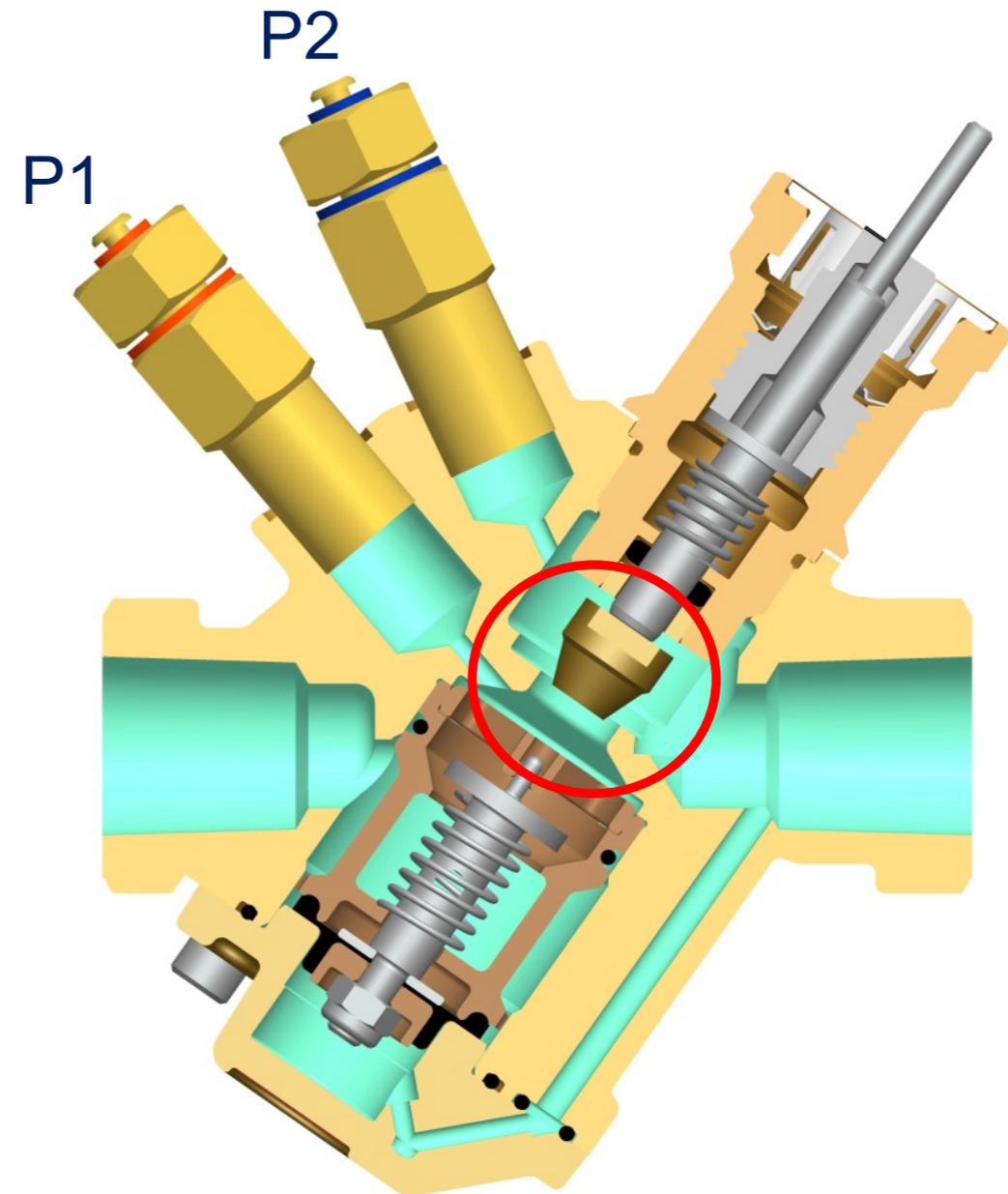
measured by integral test points

Where test points measure

P1 – P3

Δp will vary

between min & max

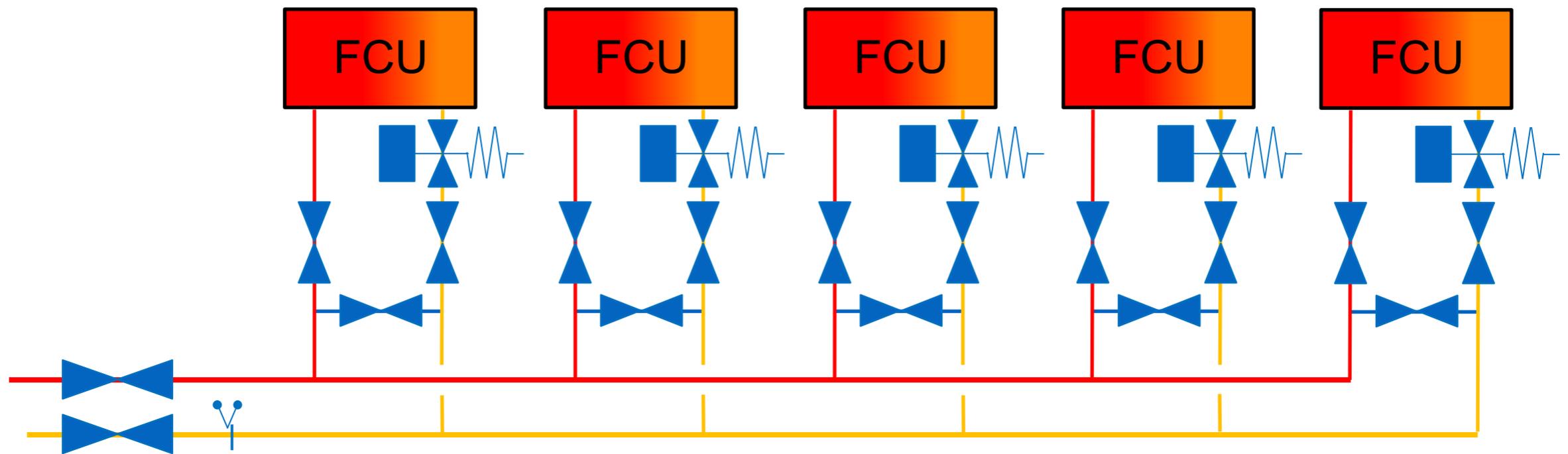


PICV Selection

Flow rate is the *main* selection criteria

Other considerations could be

- minimising pressure drop
- matching line sizes



Almost always it is flow rate that determines selection

PICV Selection

DN15 Low Flow			DN15 Standard Flow		
setting position	flow rate l/s	total Δp kPa	setting position	flow rate l/s	total Δp kPa
2	0.008	15	2	0.04	15
3	0.010	15	3	0.060	15
4	0.020	15	4	0.080	20
5	0.030	15	5	0.105	20
6	0.040	20	6	0.120	20
7	0.050	20	7	0.140	20
8	0.060	20	8	0.155	25
9	0.070	20	9	0.175	25
10	0.080	20	10	0.200	25

selection charts are available

- flow rates
- set position
- minimum Δp (differential pressure) *total loss at activation*

PICV Selection – activation point

- *activation* Δp lower than *total* Δp
- activation Δp constant
- total Δp varies

DN15 standard Flow			
setting position	flow rate l/s	total Δp kPa	activation Δp kPa
2	0.040	15	12
3	0.060	15	12
4	0.080	20	12
5	0.100	20	12
6	0.120	20	12
7	0.140	20	12
8	0.160	25	12
9	0.180	25	12
10	0.200	25	12

PICV Selection

DN15 Low Flow			DN15 Standard Flow			DN20 Standard Flow		
setting position	flow rate l/s	total Δp kPa	setting position	flow rate l/s	total Δp kPa	setting position	flow rate l/s	total Δp kPa
2	0.008	15	2	0.04	15	2	0.065	15
3	0.010	15	3	0.060	15	3	0.100	20
4	0.020	15	4	0.080	20	4	0.130	20
5	0.030	15	5	0.105	20	5	0.160	20
6	0.040	20	6	0.120	20	6	0.190	25
7	0.050	20	7	0.140	20	7	0.220	25
8	0.060	20	8	0.155	25	8	0.240	25
9	0.070	20	9	0.175	25	9	0.260	25
10	0.080	20	10	0.200	25	10	0.280	25

Example
 required flow rate 0.160l/s

between setting 8 & 9
 8.3ish

setting 5

PICV Selection

DN15 Low Flow			DN15 Standard Flow			DN20 Standard Flow		
setting position	flow rate l/s	total Δp kPa	setting position	flow rate l/s	total Δp kPa	setting position	flow rate l/s	total Δp kPa
2	0.008	15	2	0.04	15	2	0.065	15
3	0.010	15	3	0.060	15	3	0.100	20
4	0.020	15	4	0.080	20	4	0.130	20
5	0.030	15	5	0.105	20	5	0.160	20
6	0.040	20	6	0.120	20	6	0.190	25
7	0.050	20	7	0.140	20	7	0.220	25
8	0.060	20	8	0.155	25	8	0.240	25
9	0.070	20	9	0.175	25	9	0.260	25
10	0.080	20	10	0.200	25	10	0.280	25

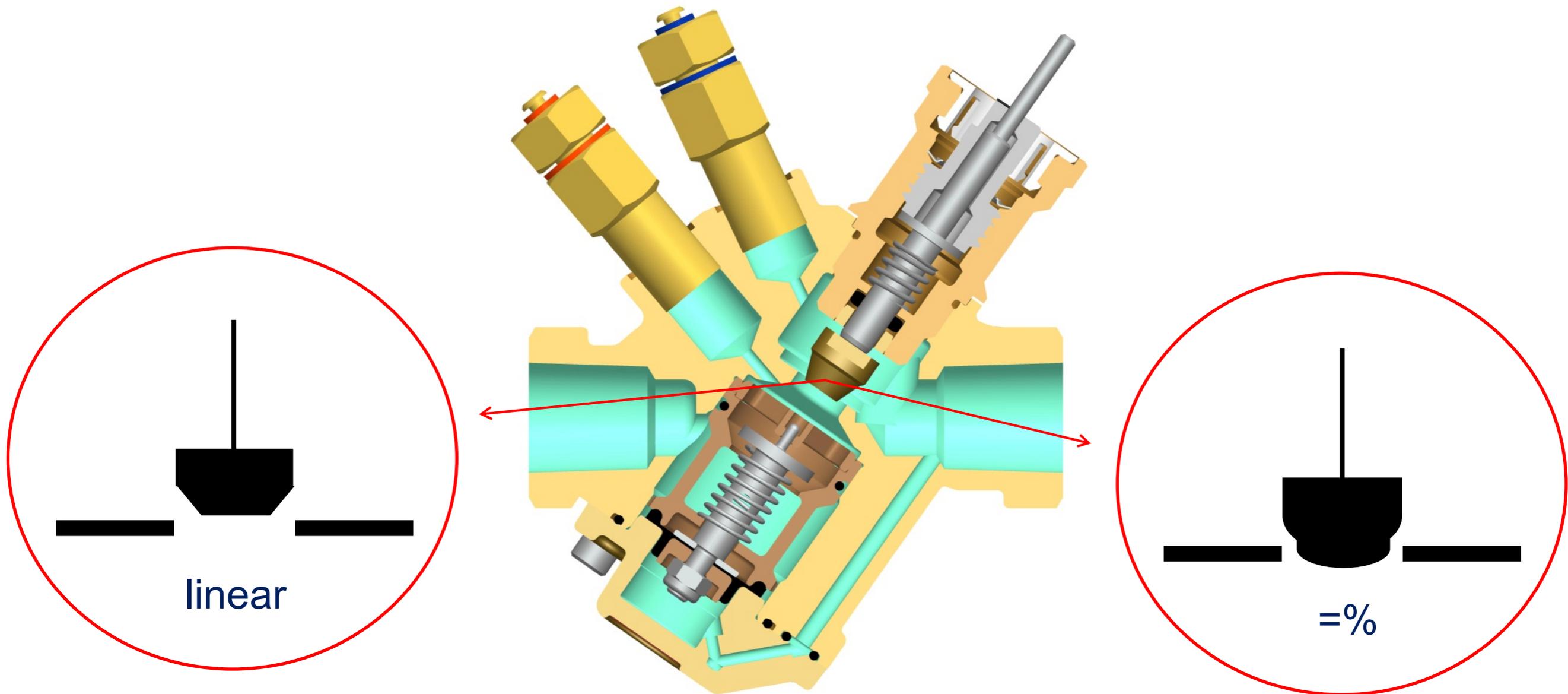
example
 required flow rate 0.160l/s

total Δp (P1 – P3)
 25 kPa

total Δp (P1 – P3)
 20 kPa

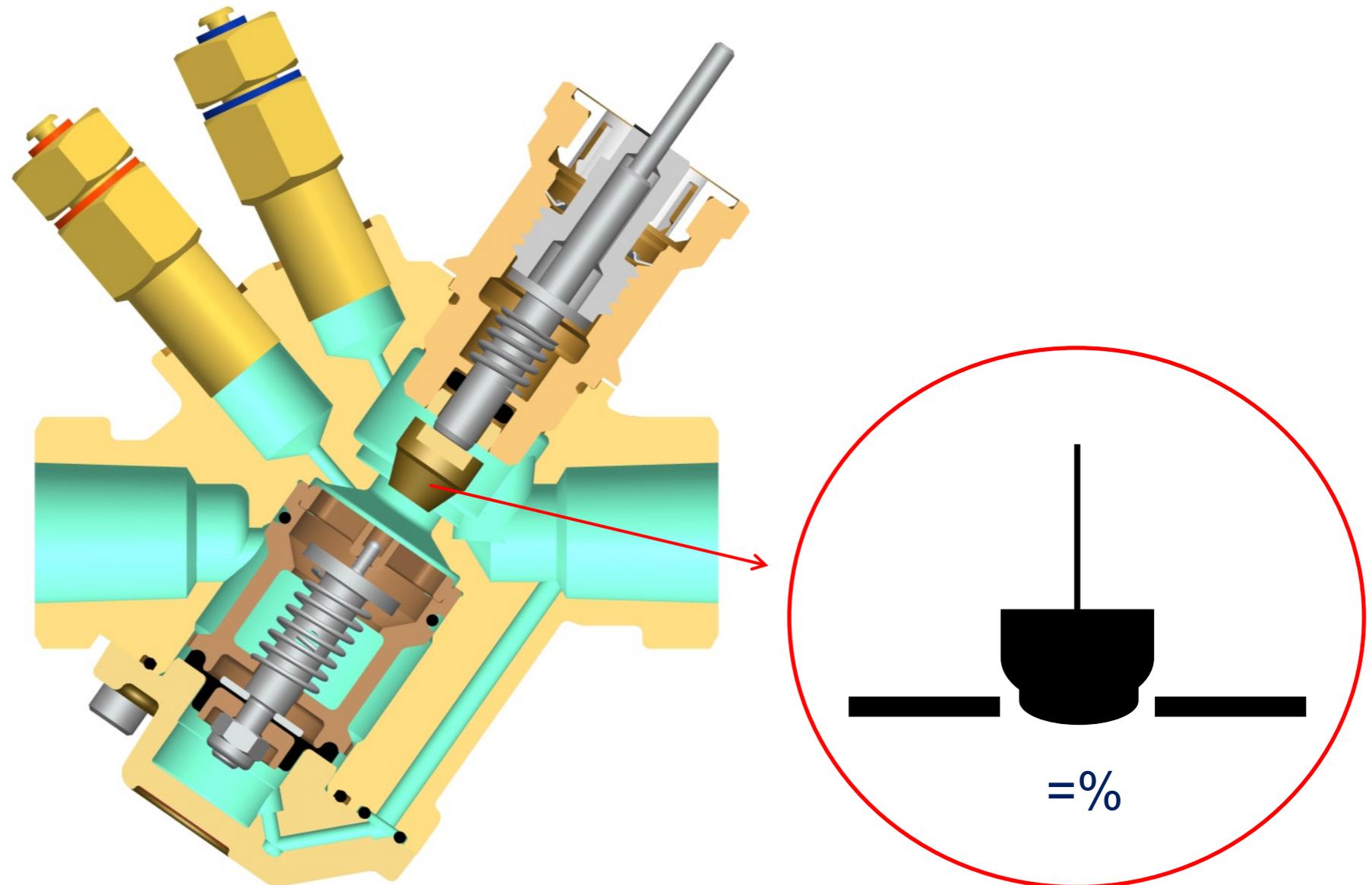
Total Δp could rise to max Δp – 350 kPa

PICV Control Characteristic

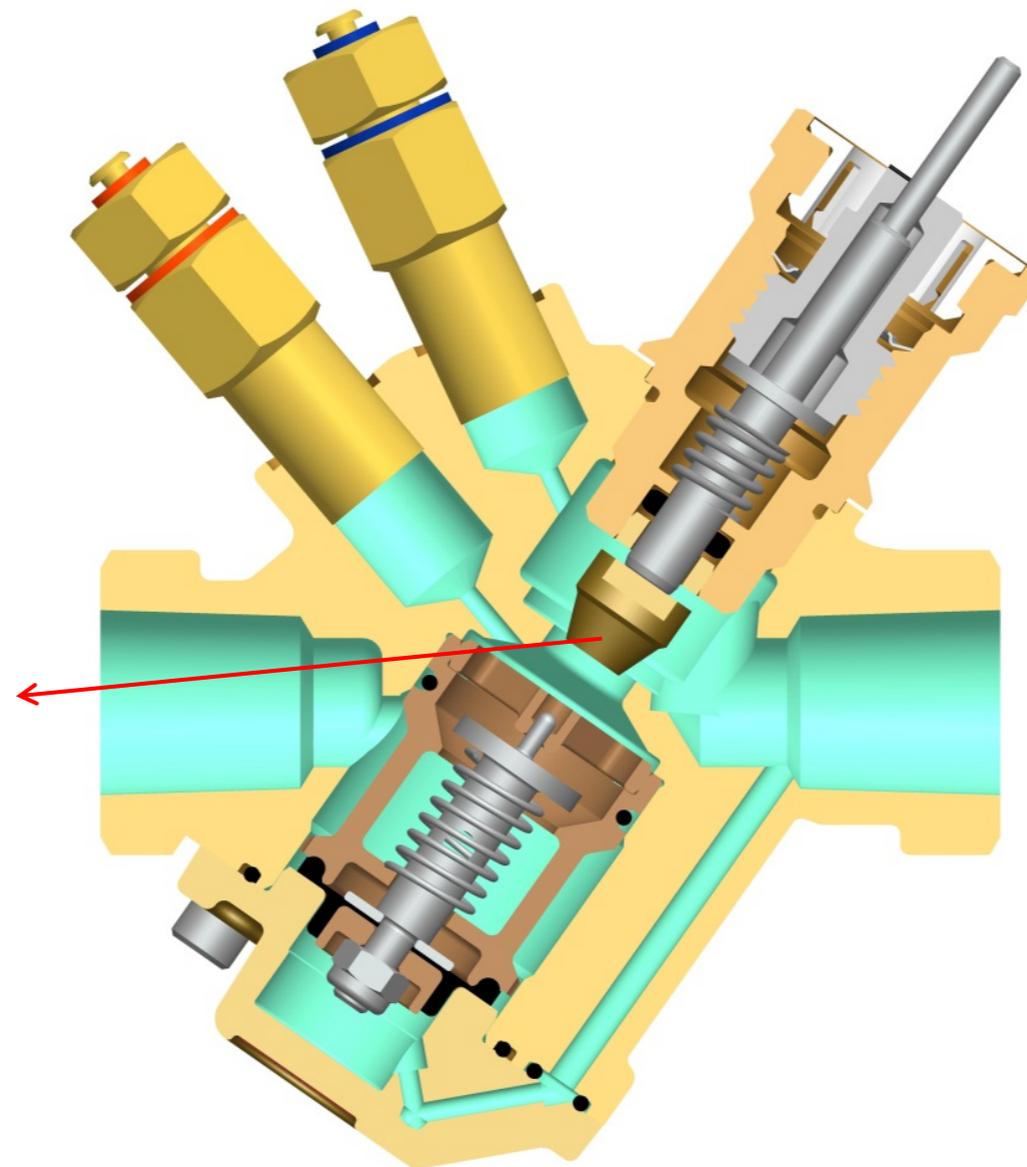
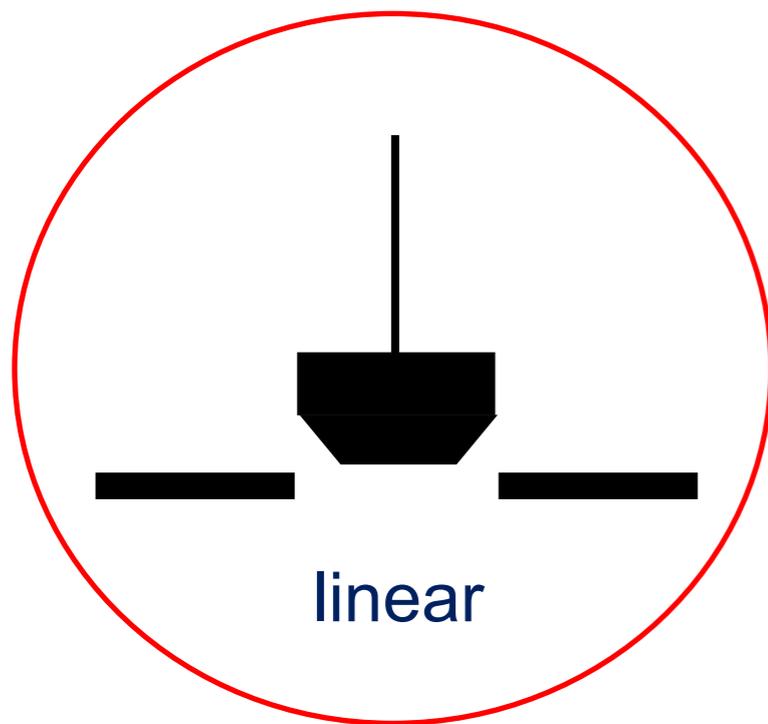


PICV Control Characteristic - =%

if stem it used to regulate flow rate
Control Characteristic
is changed at lower settings



PICV Control Characteristic - linear



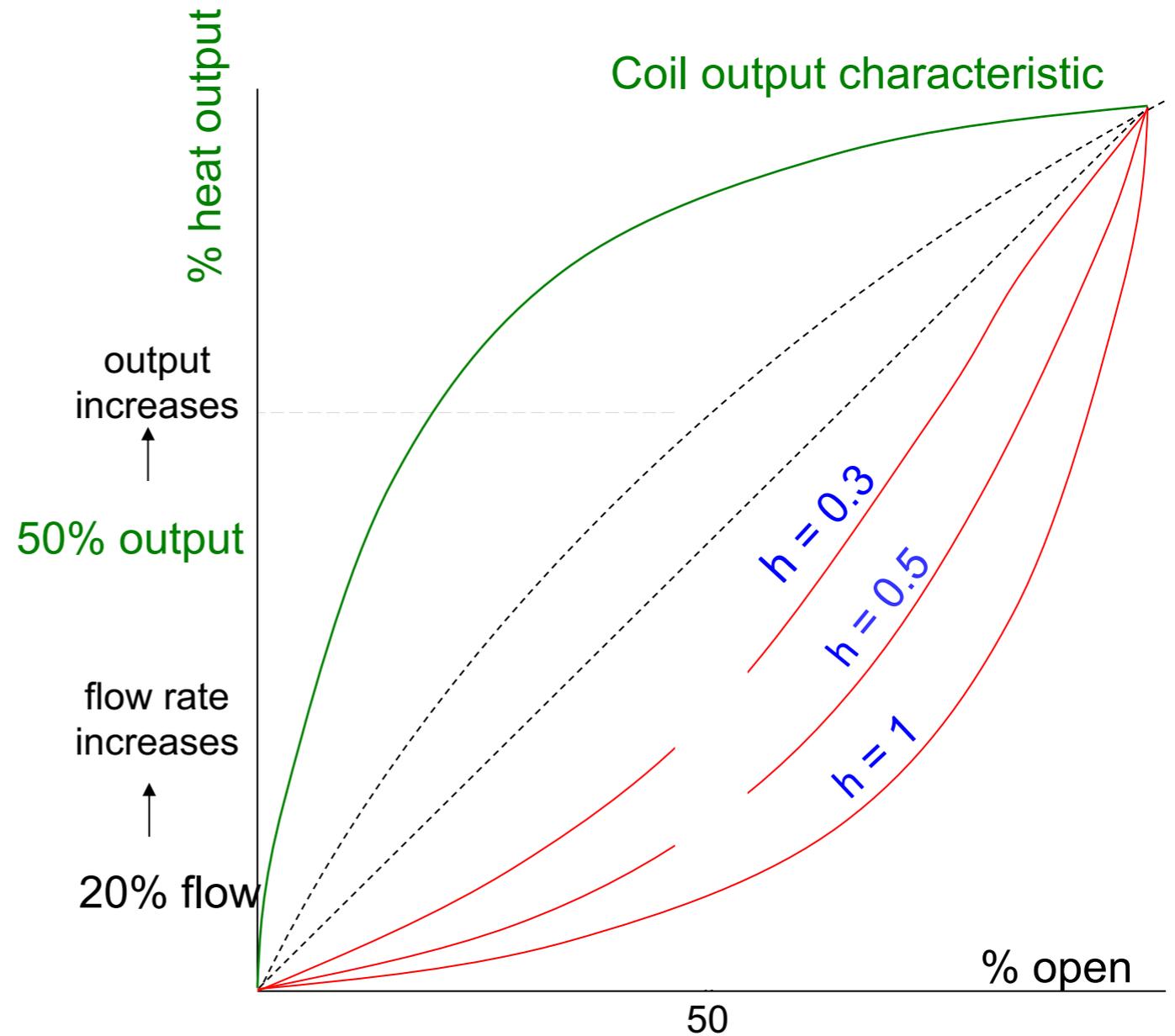
If stem it used to regulate flow rate
Control Characteristic
is **NOT** changed at
lower settings

PICV Control Characteristic

Equal percentage control valves are designed with a

$$h = 1$$

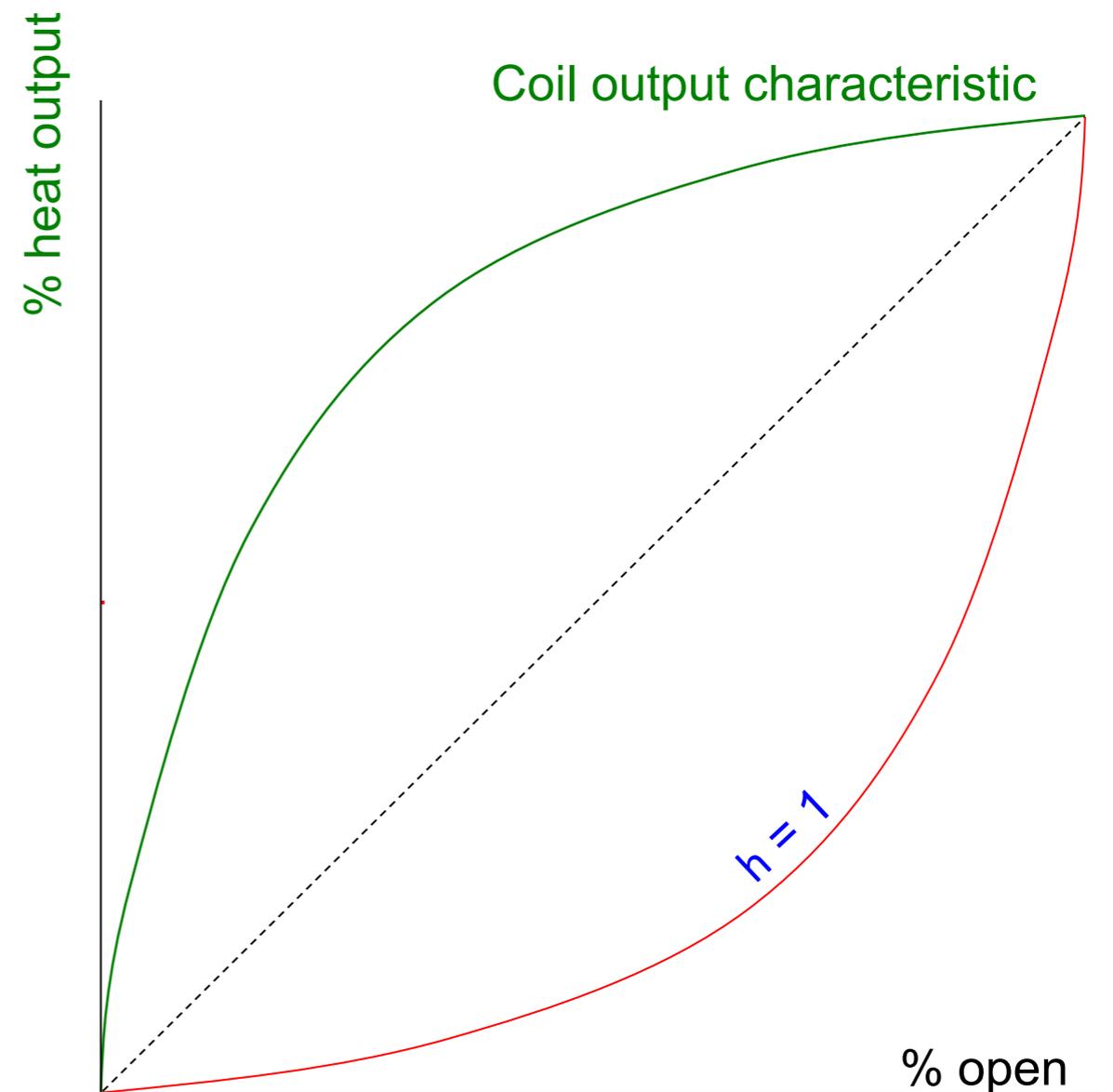
Mirror image of coil characteristic



PICV Control Characteristic - =%

- Establish a direct relationship between open position & *heat output*
- 50% valve opening = 50% heat output

Dynamic Balancing

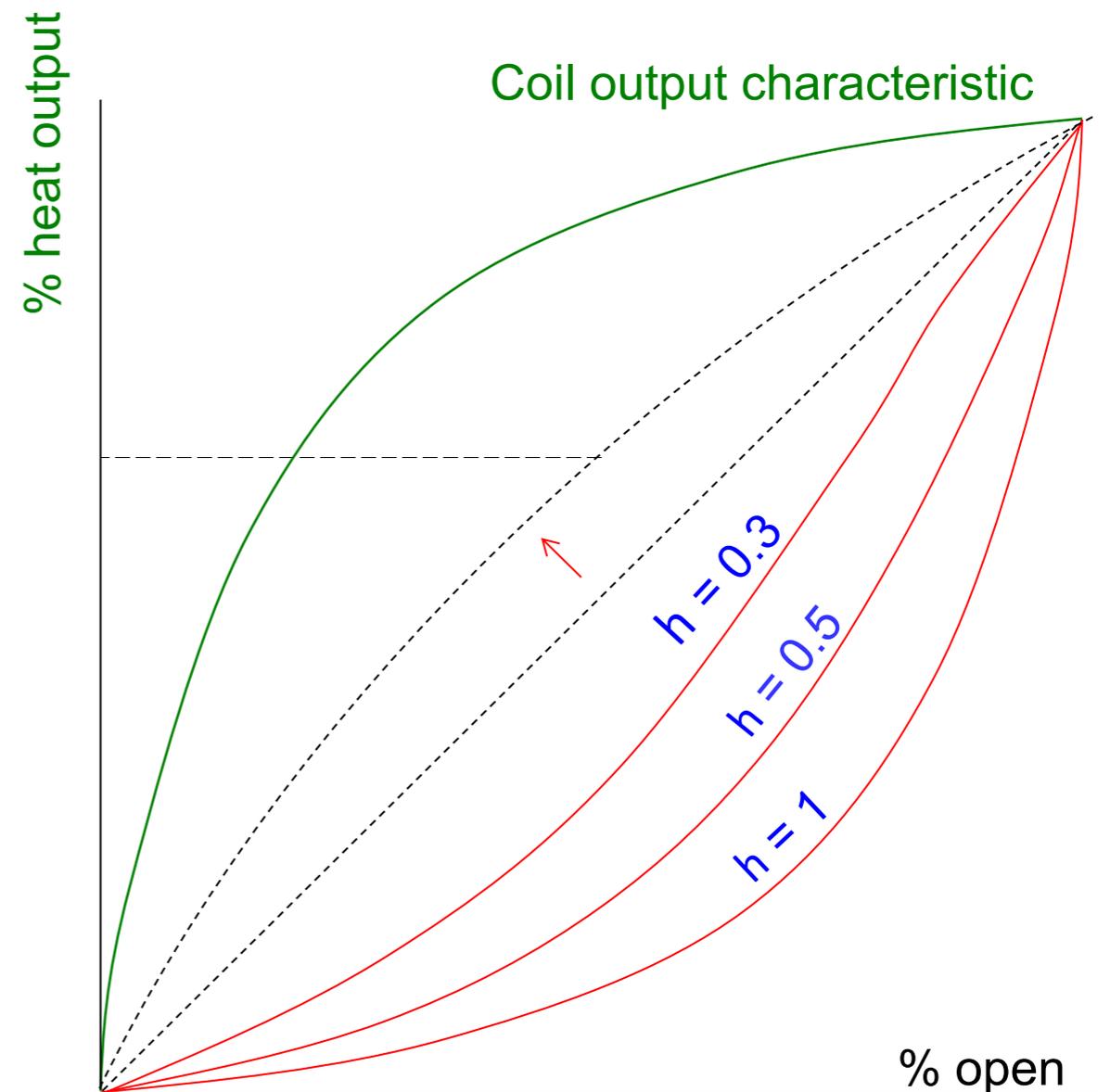


PICV Control Characteristic - =%

- Where stem used to regulate flow rate
- Changes control characteristic

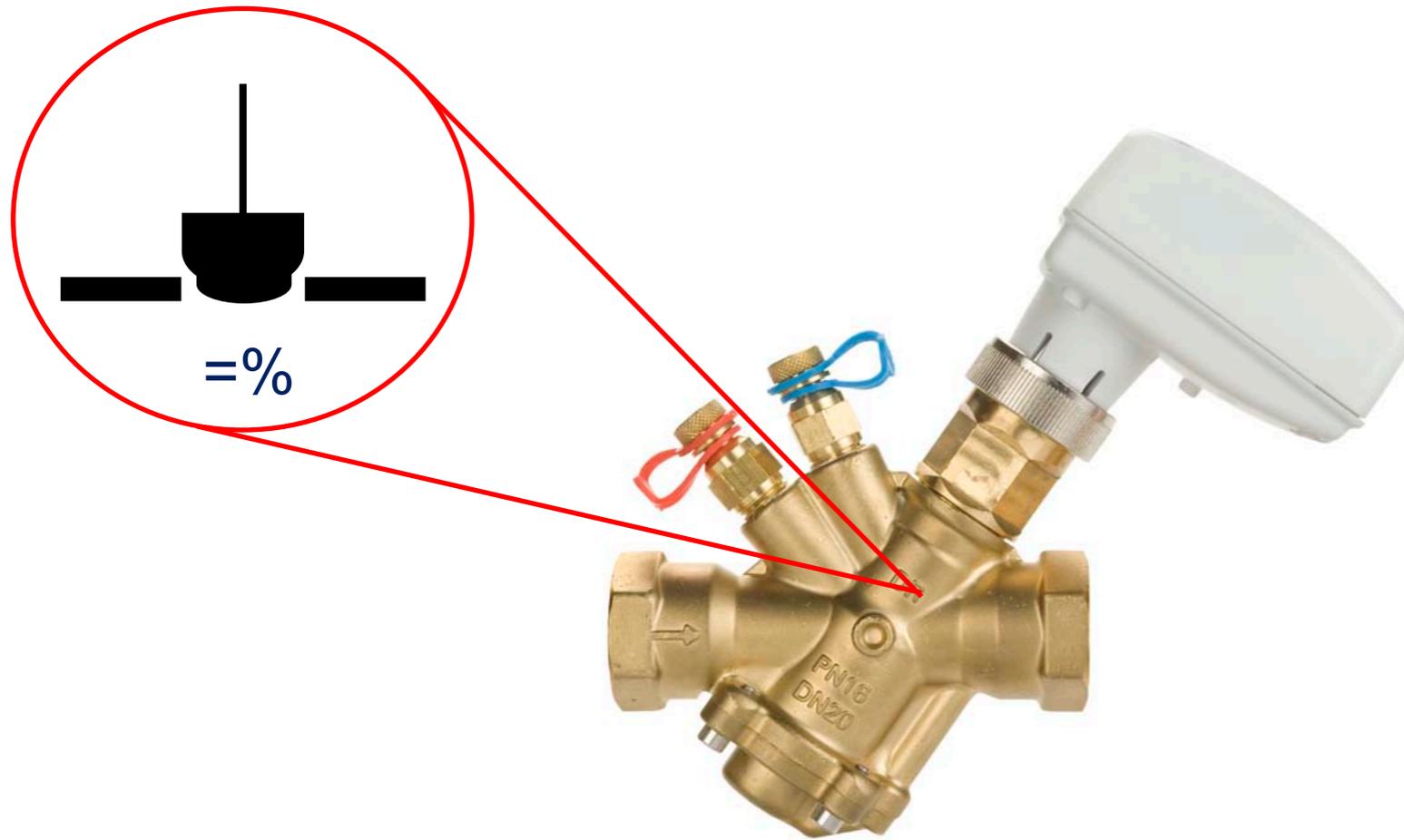
*combined 'linear' position moves
due to effect of valve
characteristic*

Dynamic Balancing

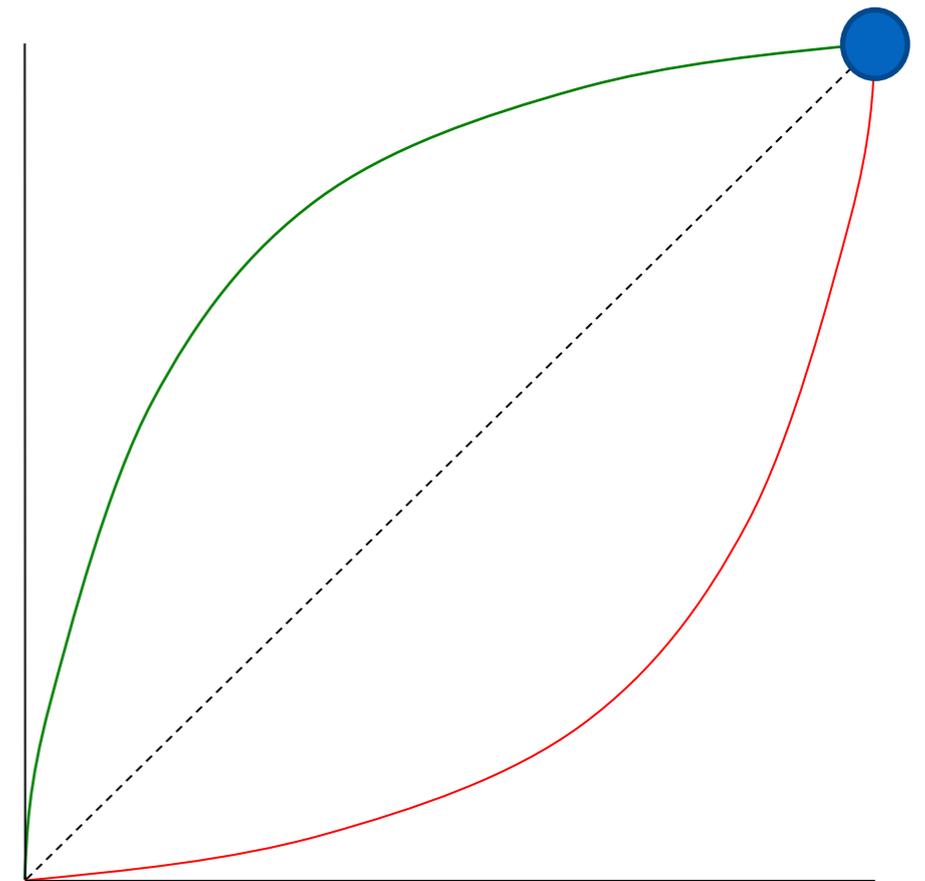


PICV Control Characteristic - =%

Dynamic Balancing

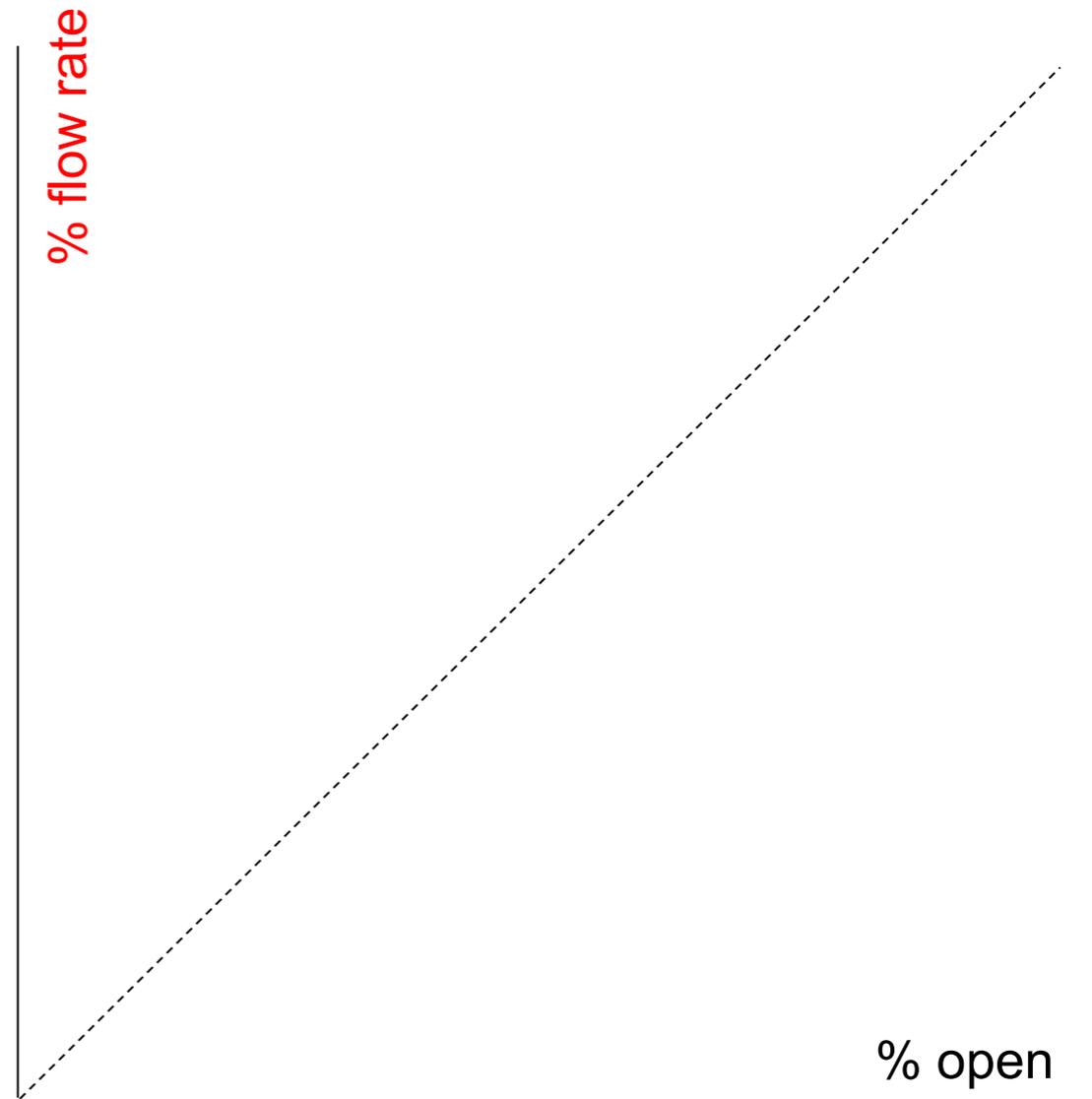


'Linear' control actuator giving equal percentage characteristic

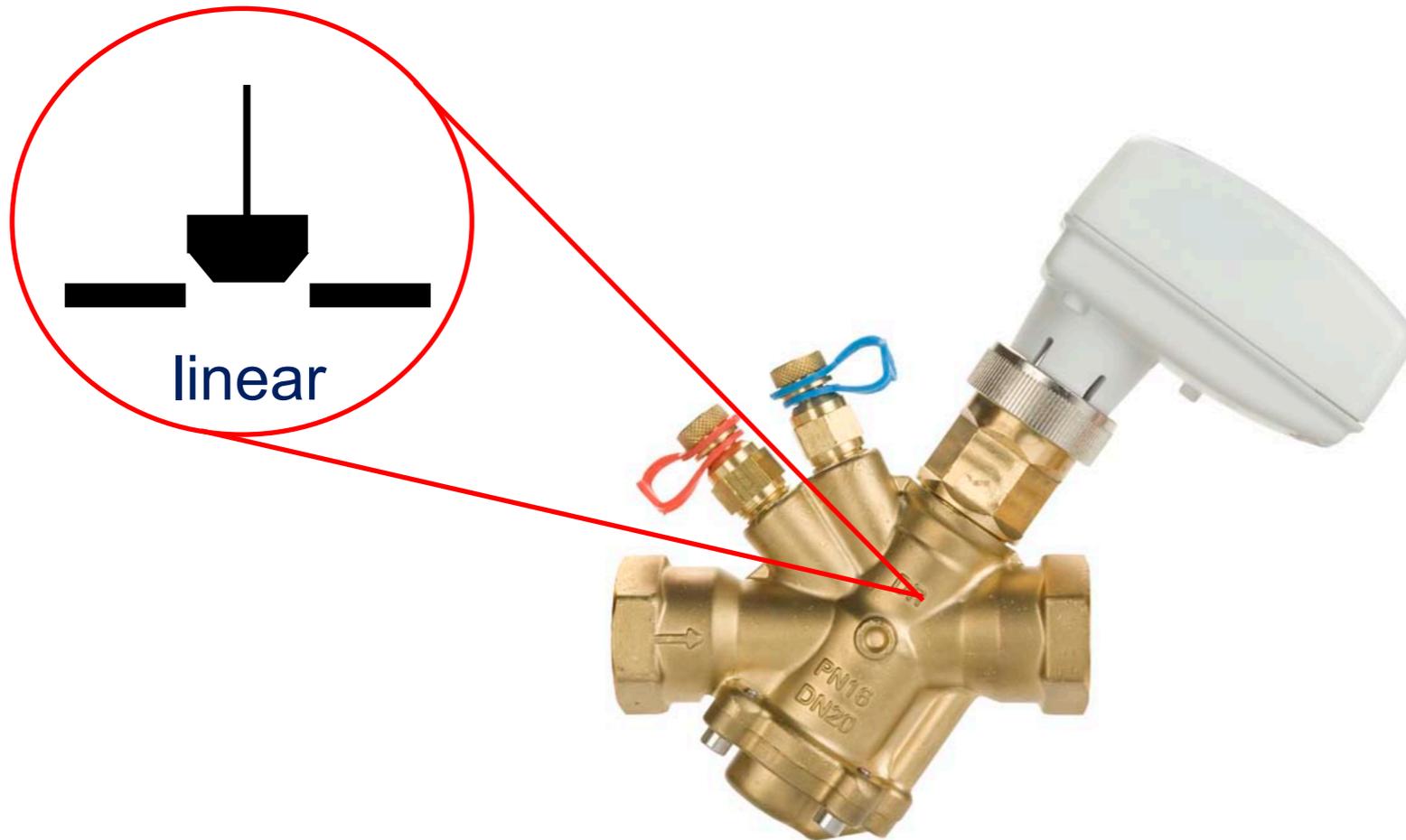


PICV Control Characteristic - linear

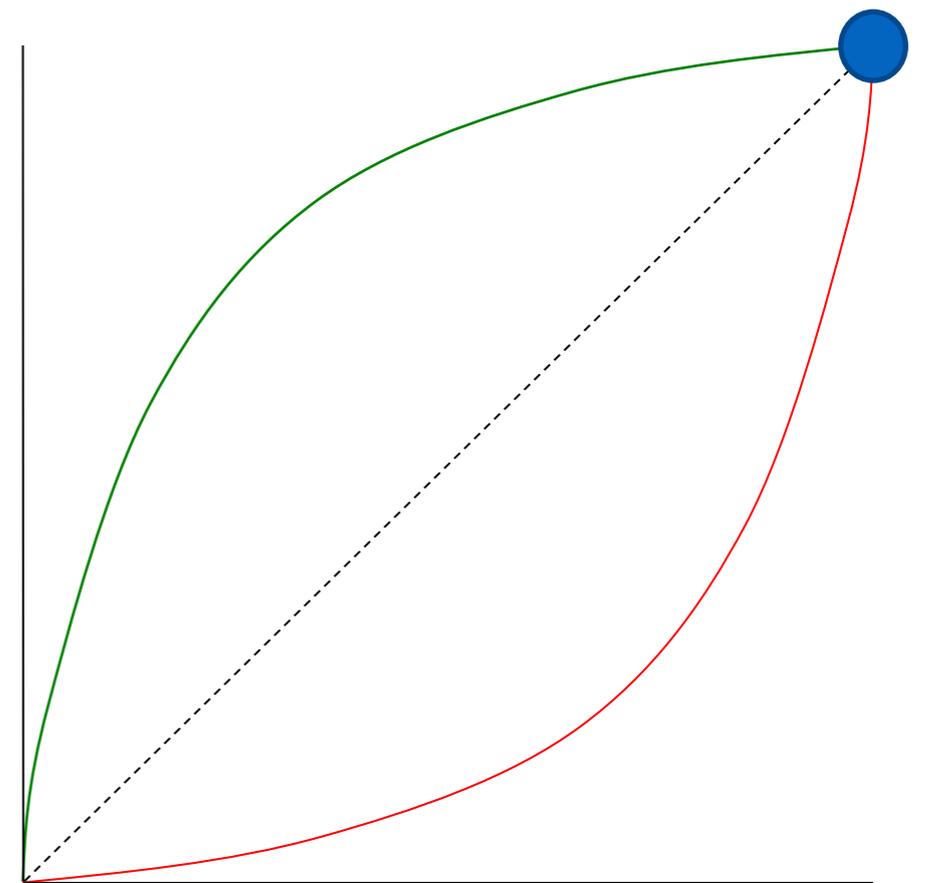
- Establish a direct relationship between open position & *flow rate*
- 50% valve opening = 50% *flow rate*
- Not effected by flow regulation



PICV Control Characteristic - linear



'Equal Percentage' control actuator giving equal percentage characteristic



Variable Volume System

At maximum pump turndown, typically 10 - 20%, consideration needs to be given to branches to ensure

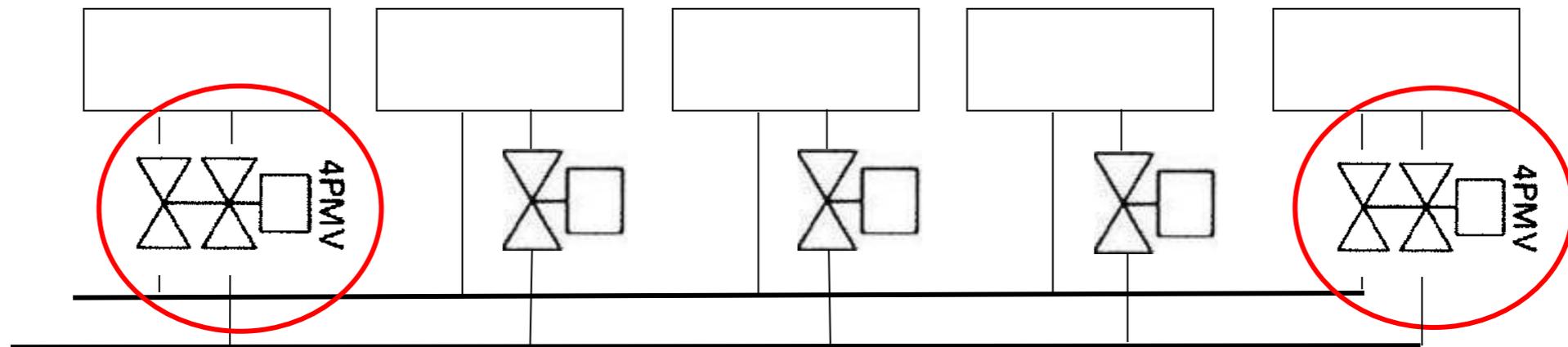
- pump flow at minimum load
- circulation of water treatment
- ready supply of heating / chilled water

Dynamic Balancing of the System

Possible solution

End terminal could have a 3 or 4 port control valve

- on larger circuits additional 3 or 4 ports could be added



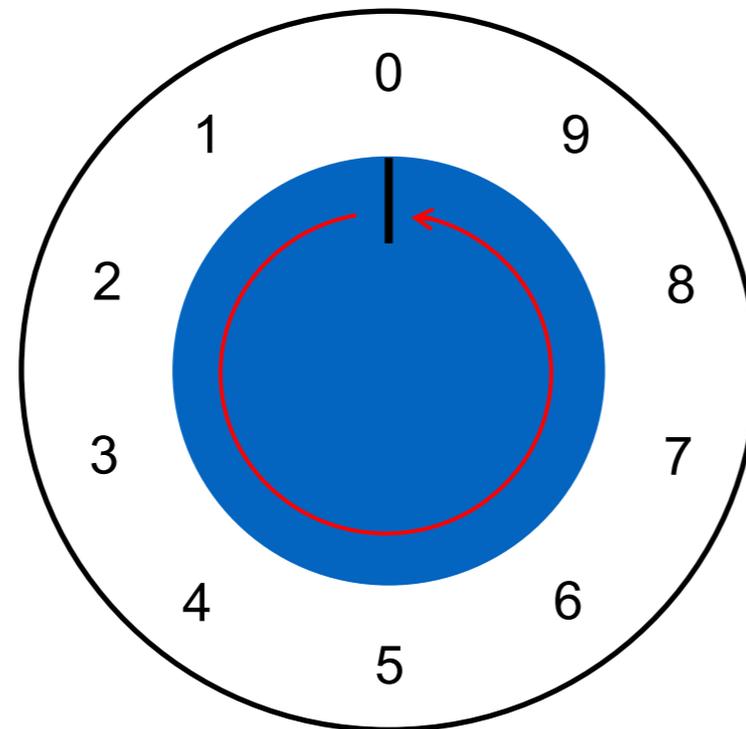
Flow Accuracy

Different factors affect accuracy

- pre-set position
- available pump pressure
- actuator control

Accuracy is a combination of all factors

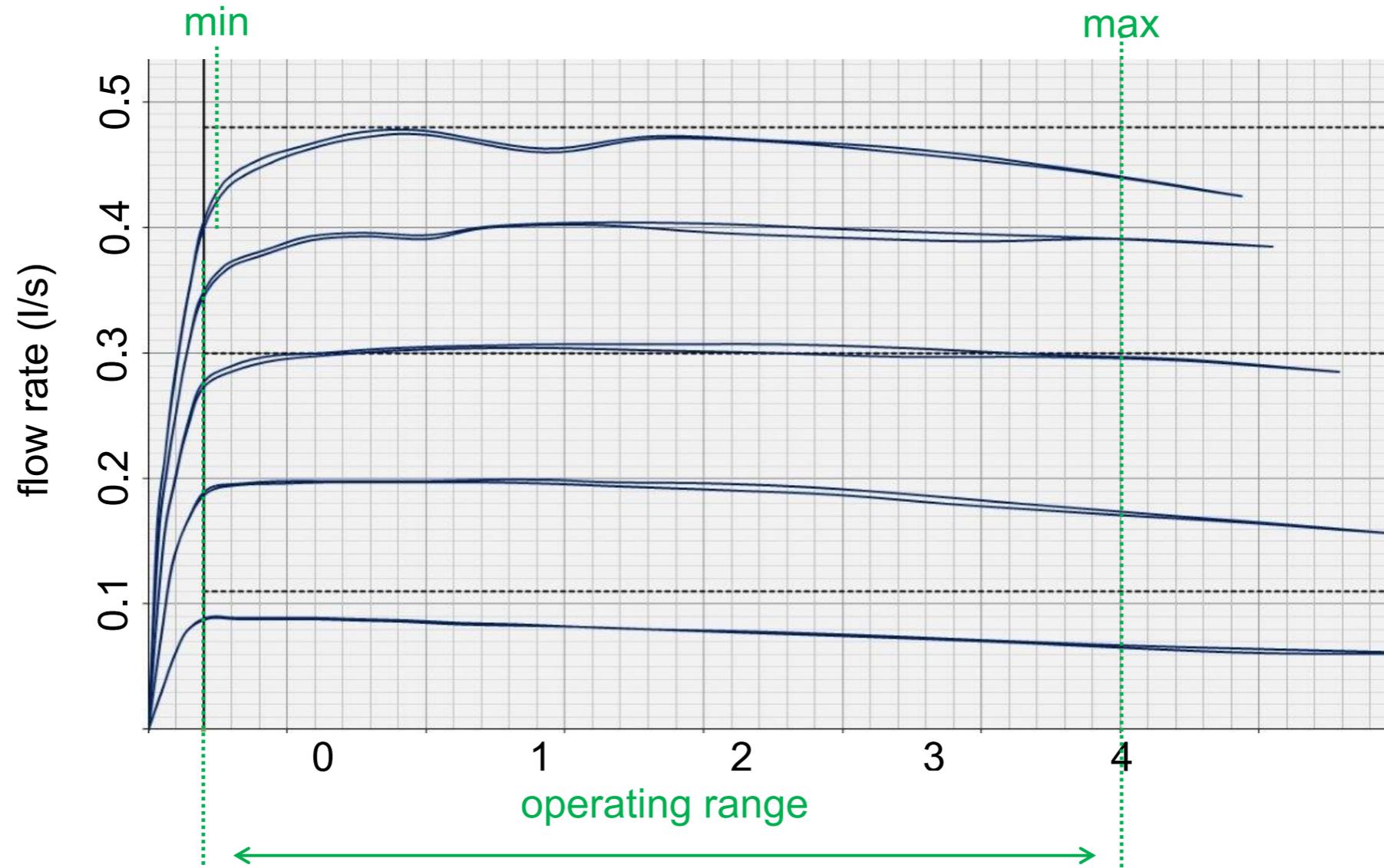
Flow Accuracy – Pre-set Position



Aligning dial with scale

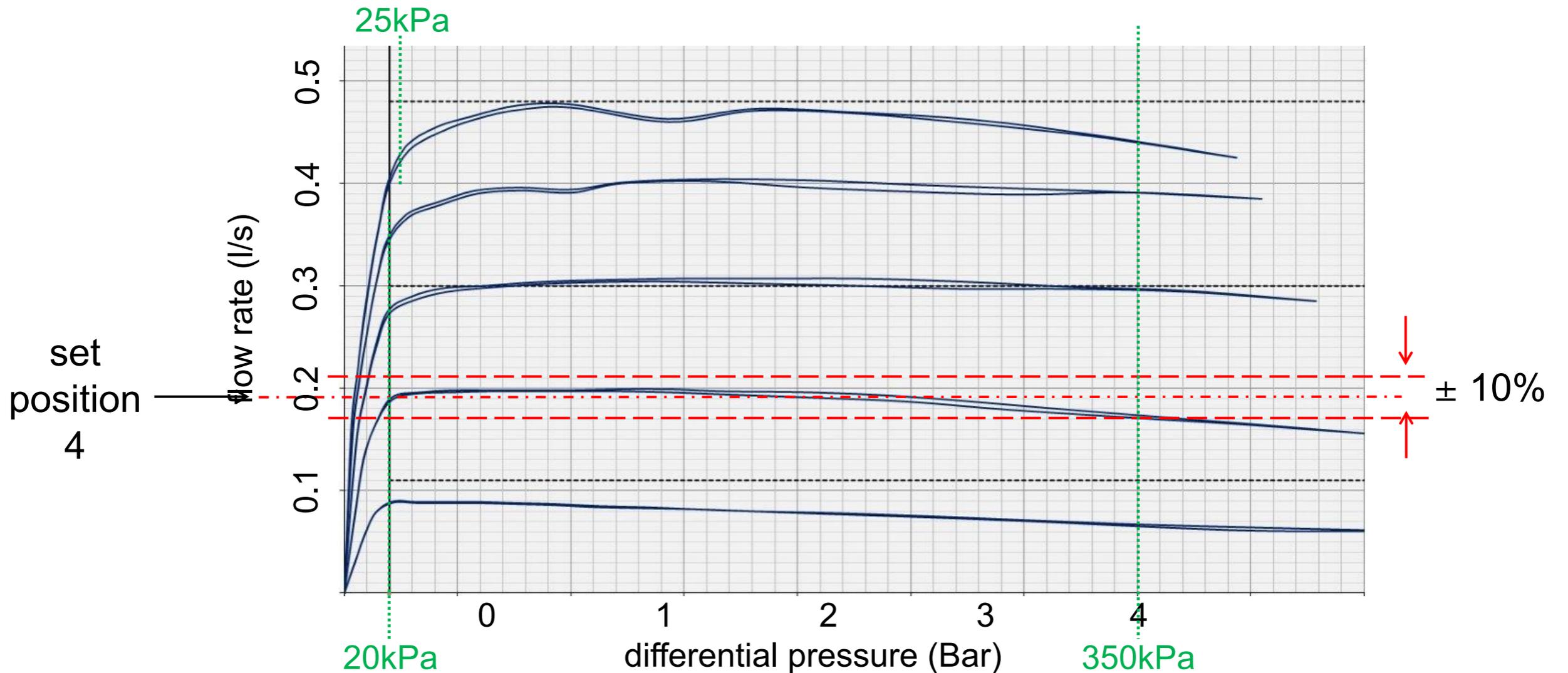
Pre-set position accuracy can be improved by the installation of a FMD

Flow Accuracy – Available Pump Pressure



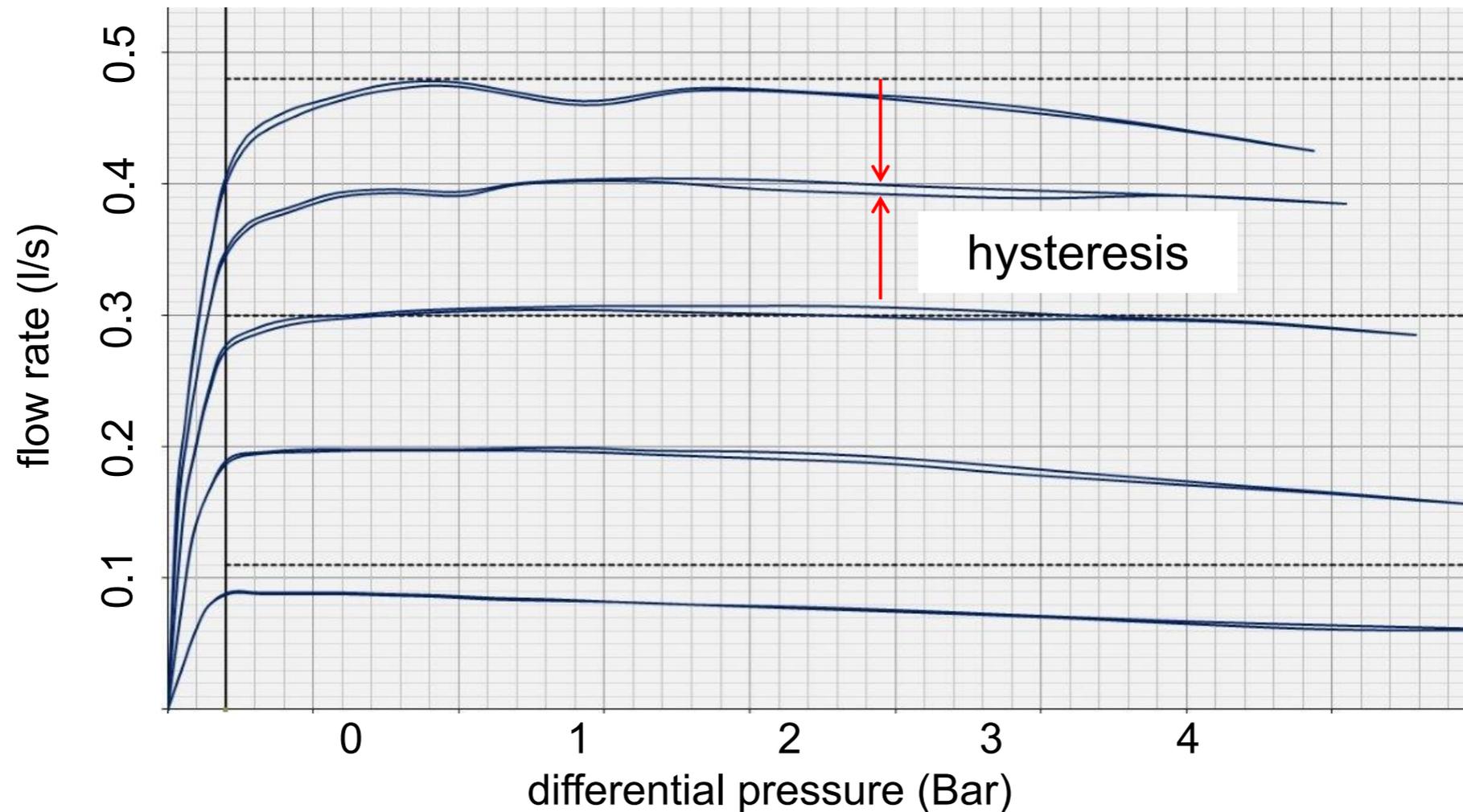
As pump pressure varies flow rate varies

Flow Accuracy – Available Pump Pressure



As pump pressure varies flow rate varies

Flow Accuracy – Rising / Falling Pressure



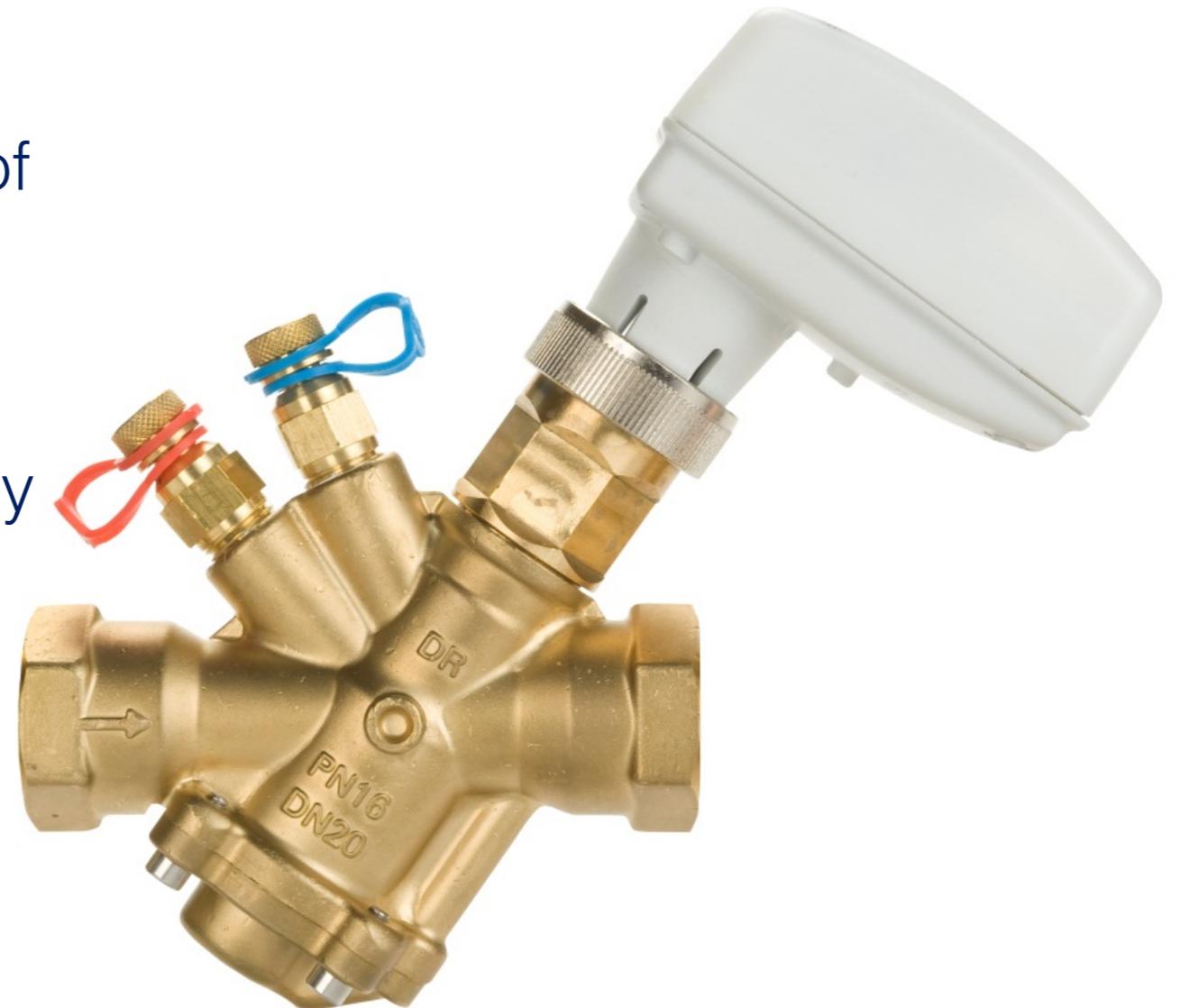
Hysteresis is relatively low but need to be considered and understood

Flow Accuracy – Actuator

Installed PICVs are a combination of

- PICV
- Actuator

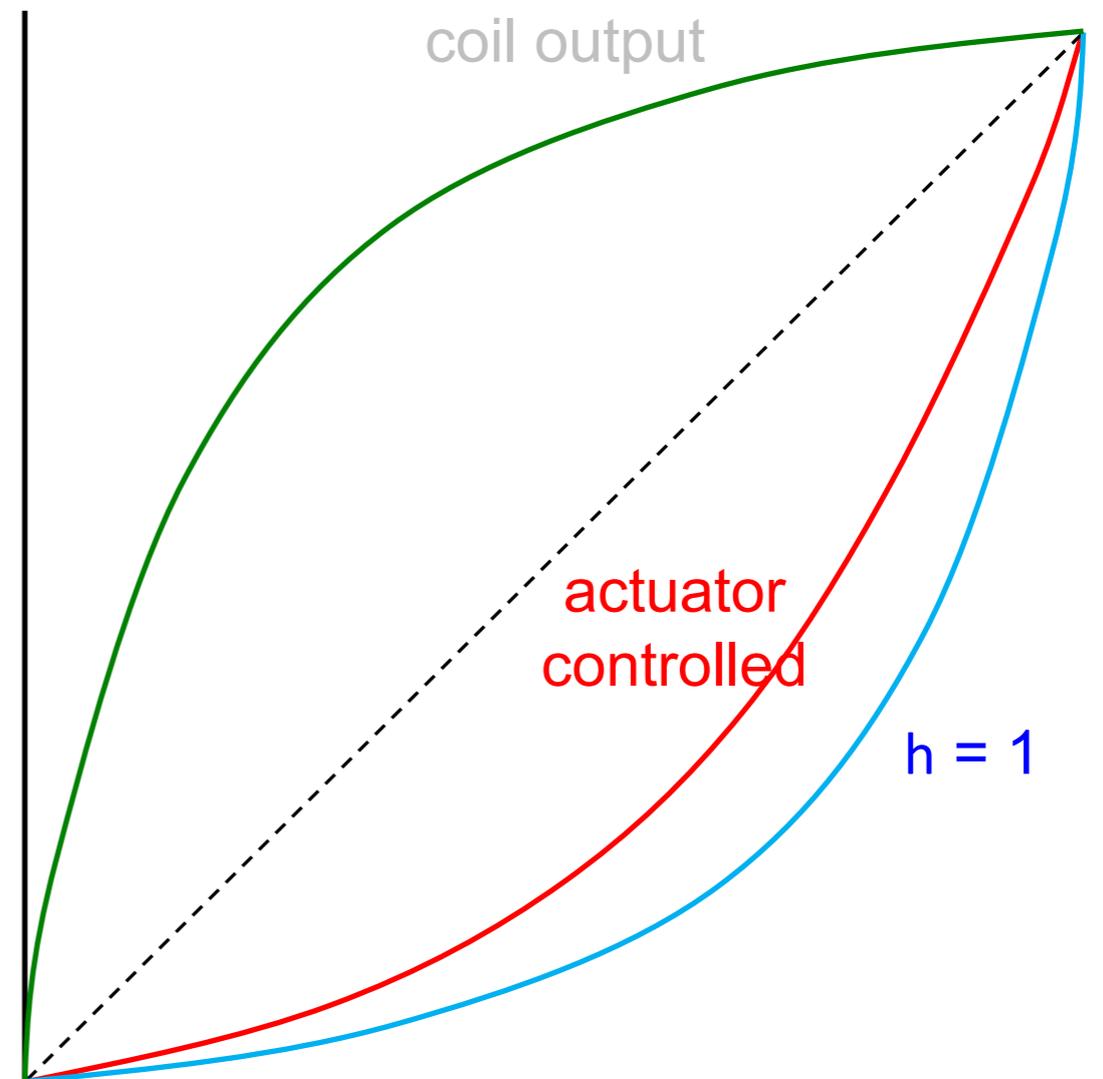
so we should consider the assembly
and not the standalone PICV



Consider as a 'matched' pair

Flow Accuracy – Actuator

- PICV can perform well as a stand alone valve
- But when actuator is fitted performance of valve can be undermined



Actuators

Actuators are divided into 2 types

- Thermal
- Electro-mechanical

And then by control characteristic

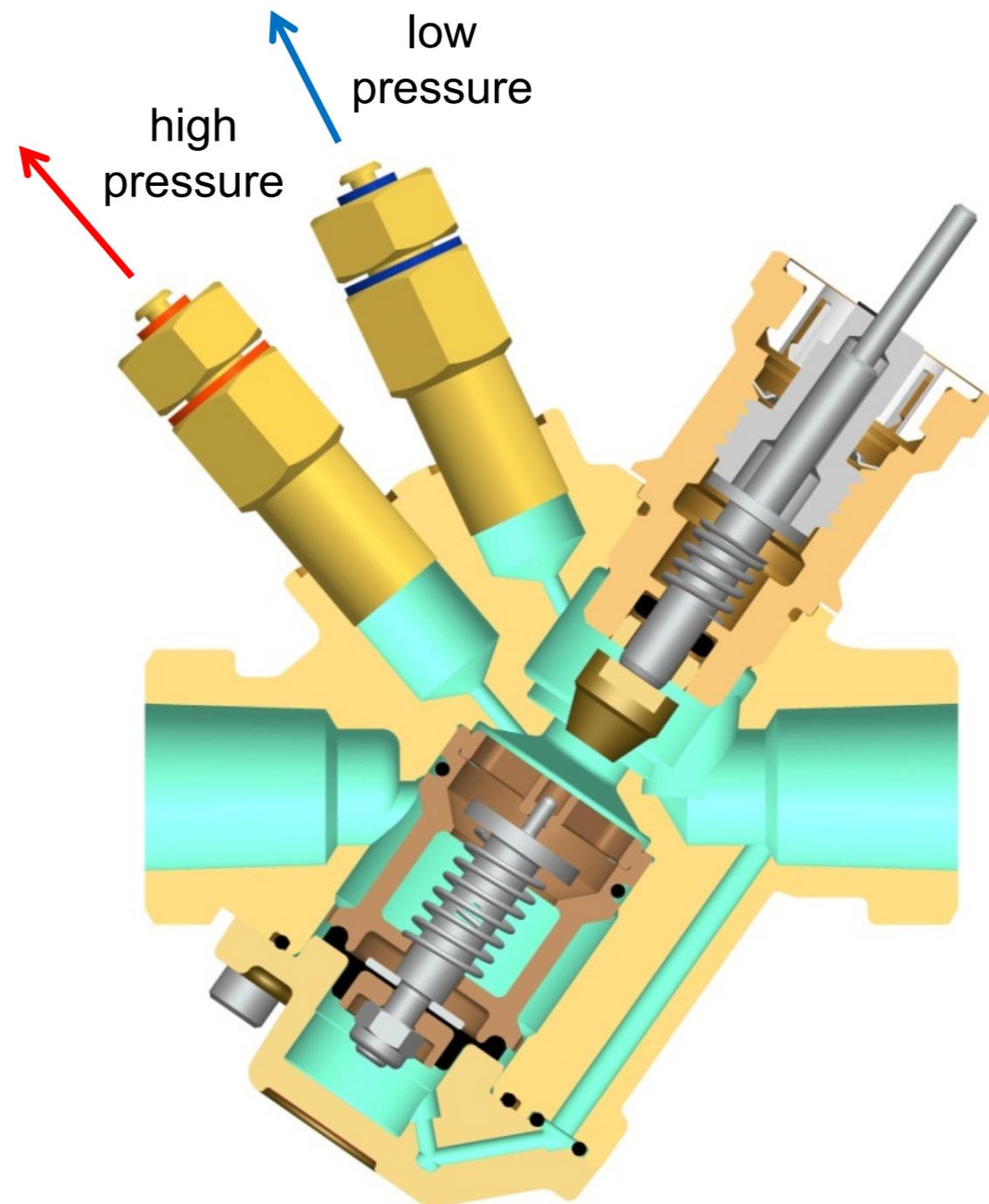
- On / Off
- Modulating

PICV Commissioning

PICVs are set to give the required flow rate, there is no commissioning required for the PICV

Commissioning Engineers are required to set the pump speed to ensure that the *'least favoured'* (index) PICV generates at least the minimum required differential pressure

if the least favoured PICV has sufficient different pressure, all other PICVs must have greater differential pressure



Summary

- Change in system design to variable flow controlled by 2 port control valve resulting in pump energy saving
- Fluctuation in system pressure undermines control valve authority
- DPCV installed into sub-circuits to 'protect' control valves from fluctuating pressure to maintain control valve authority
 - terminal units commissioned by conventional proportional method
 - branches commissioned by use of 'Companion' Valve & DPCV
 - branches commissioned independently of each other
- PICVs installed on terminal unit
 - replacing static commissioning valves / 2 port control valve / DPCV